



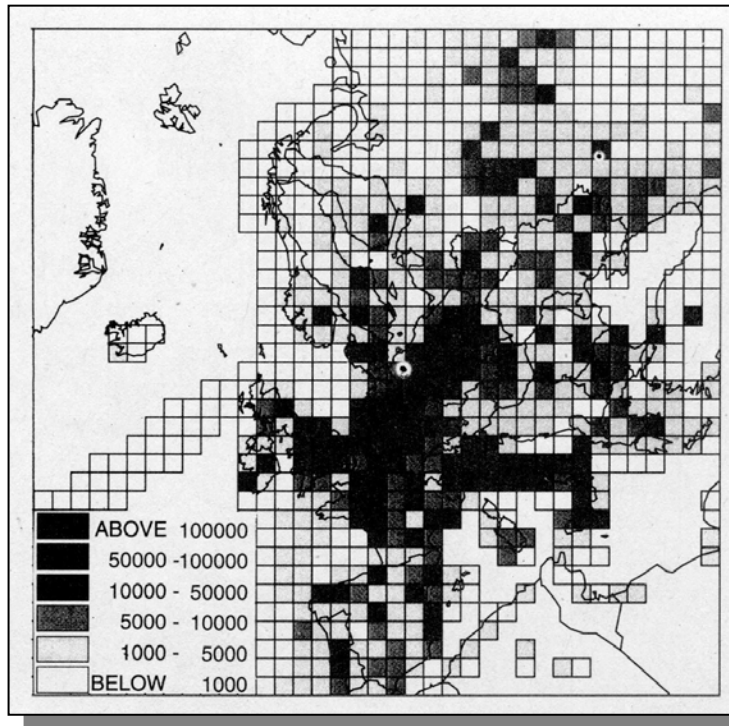
# NITROGEN #1

- $\text{NO}_x$  and  $\text{NH}_3$  emissions,  $\text{NO}_x$  deposition
- Nitrogen in fuels
- Formation and reduction of  $\text{NO}_x$  during burner combustion
- Low  $\text{NO}_x$  technology : low  $\text{NO}_x$  burners, fuel/air staging, ...
- Flue gas treatment for  $\text{NO}_x$  reduction: SCR, SNCR, other

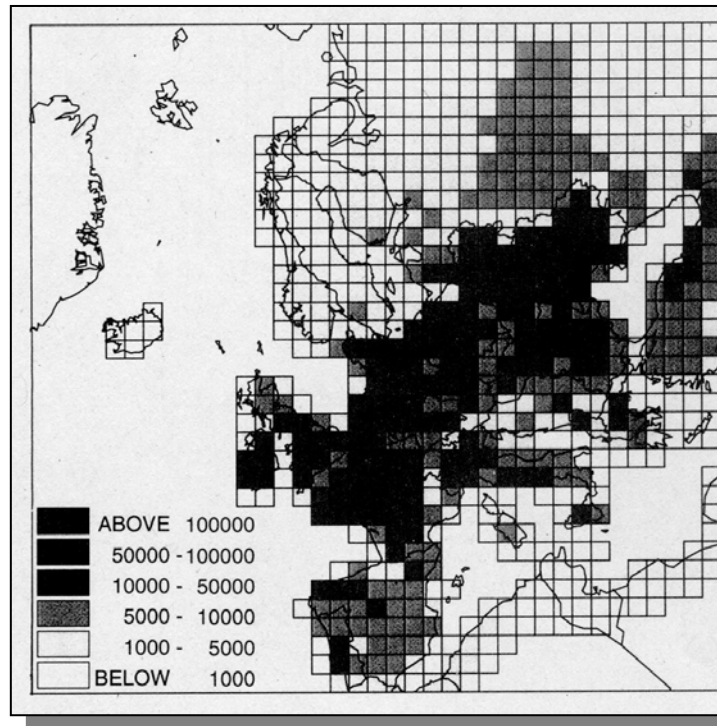
*NOTE :  $\text{NO}_x = \text{NO} + \text{NO}_2$*

*see: [www.hut.fi/~rzevenbo/gasbook](http://www.hut.fi/~rzevenbo/gasbook)*

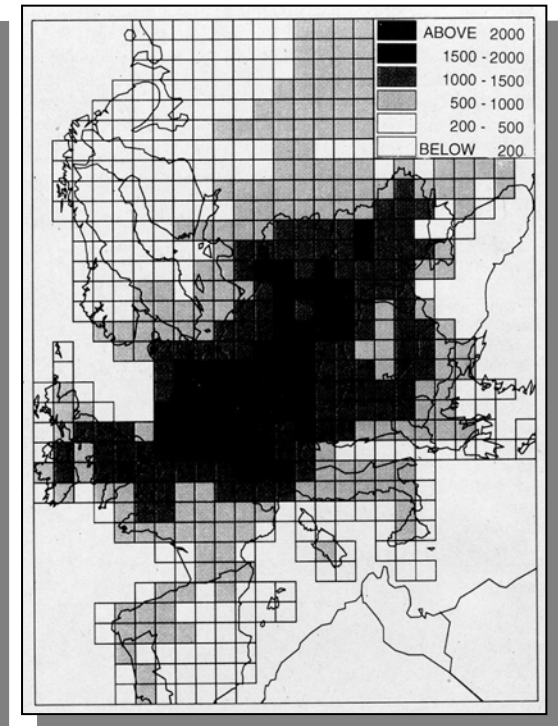
# Nitrogen emissions and deposition in Europe



NO<sub>x</sub> emissions 1994  
(tonnes N)

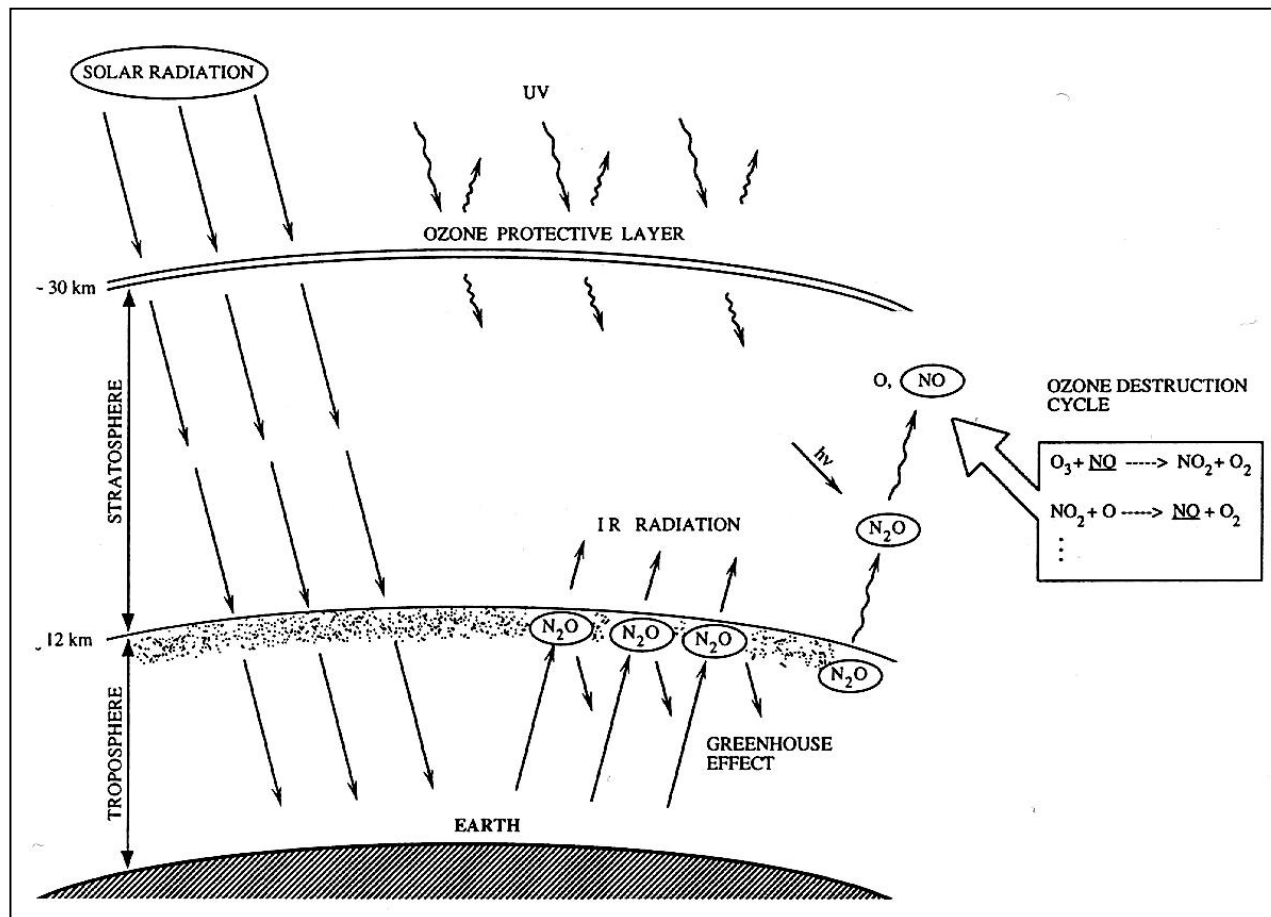


NH<sub>3</sub> emissions 1994  
(tonnes N)

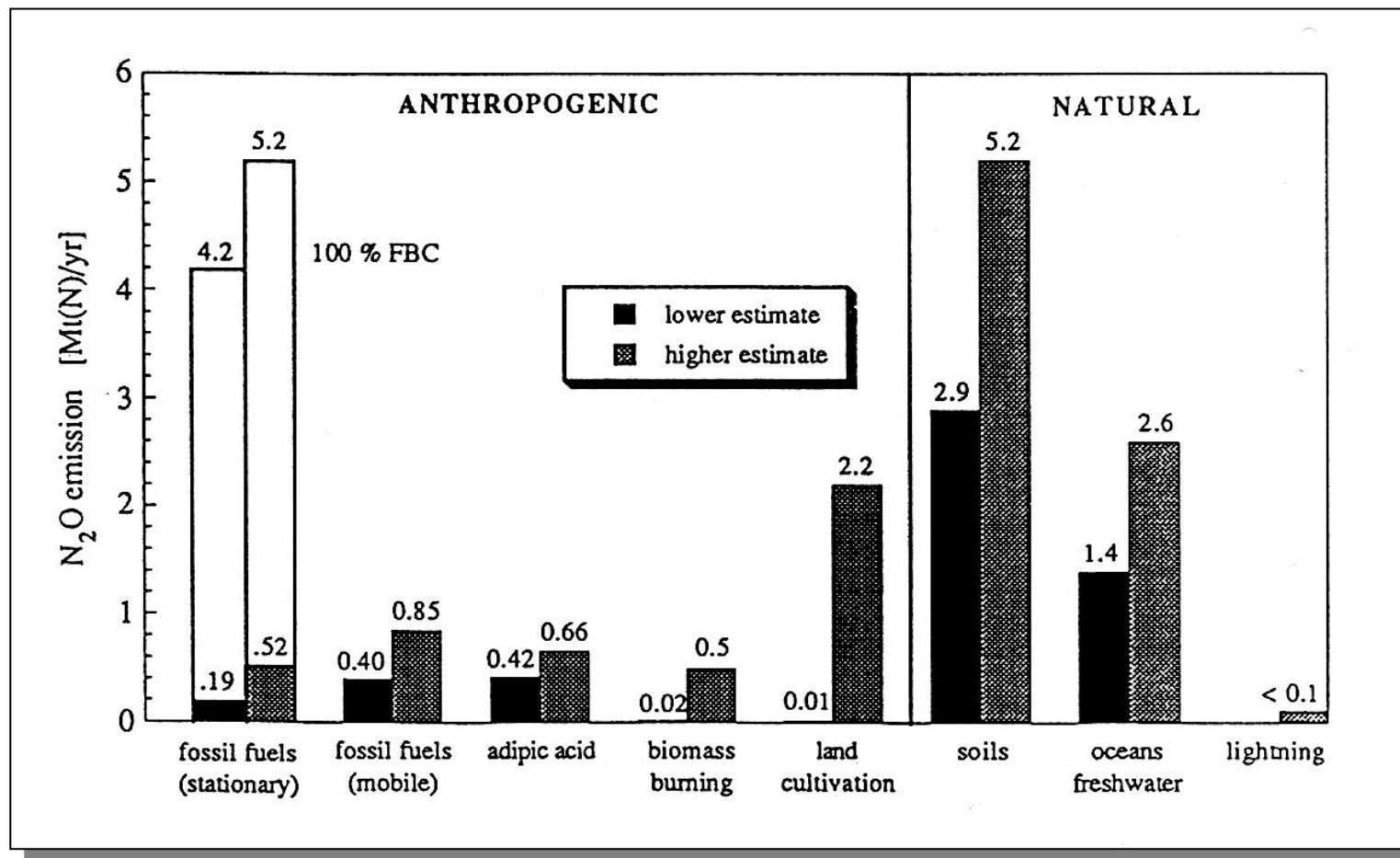


NH<sub>3</sub> + NO depositions  
1994 (mg N/m<sup>2</sup>)

# $N_2O$ as greenhouse gas and in ozone layer depletion



## Global sources of $N_2O$





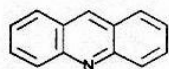
## Emissions of nitrogen compounds and human activities

Sources for NO <sub>x</sub>	Traffic	~60 %
	Fossil fuel-fired heat and power	~30 %
	Industry	~10 %
Sources for NH <sub>3</sub>	Agriculture	~80 %
Sources for N <sub>2</sub> O	Fossil fuel-fired heat and power	~30 %
	Forest fires, landgain, . . . .	~60 %
	Industry ( <i>e.g.</i> adipic acid production)	~10 %

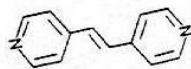




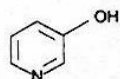
### Pyridinic-type



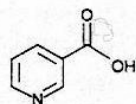
acridine or  
2,3,5,6-dibenzo-  
pyridine



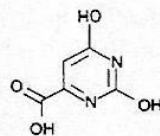
1,2-bis (4-pyridyl)-  
ethane



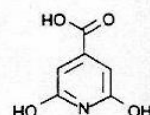
3-pyridol or  
3-hydroxypyridine



nicotinic acid or  
3-pyridinecarboxylic  
acid

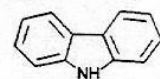


orotic acid or  
6-uracilcarboxylic  
acid

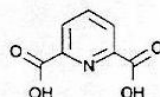


citrazinic acid or  
2,6-dihydroxy-4-pyridine-  
carboxylic acid

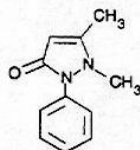
### Pyrrole-type



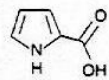
carbazole or  
dibenzopyrrole



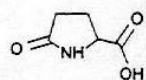
dipicolinic acid or 2,6-  
pyridinedicarboxylic acid



antipyrine or 2,3-  
dimethyl-1-phenyl-  
5-pyrazolone

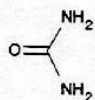


2-pyrrolecarboxylic  
acid

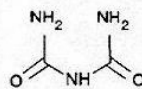


DL-pyrroglutamic  
acid or DL-5-pyrroldione-  
2-carboxylic acid

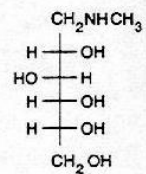
### Amino-type



urea



biuret or  
N-carbamoyurea



meglumine or  
N-methyl-D-glucamine

## Nitrogen-containing structures in solid fossil fuels and biomass

	C	H	N	O	O/N atomic ratio
Acridine	87.1	5.1	7.8	—	—
1,2-Bis(4-pyridyl)ethane	78.3	6.5	15.2	—	—
3-Pyridol	63.2	5.3	14.7	16.8	1.1
Nicotinic acid	58.5	4.1	11.4	26.0	2.3
Orotic acid	38.5	2.6	17.9	41.0	2.3
Citrazinic acid	46.5	3.2	9.0	41.3	4.6
Dipicolinic acid	50.3	3.0	8.4	38.3	4.6
Carbazole	86.2	5.4	8.4	—	—
Antipyrine	70.2	6.4	14.9	8.5	0.6
2-Pyrrolicarboxylic acid	54.1	4.5	12.6	28.8	2.3
DL-Pyrroglutamic acid	46.5	5.4	10.9	37.2	3.4
Urea	20.0	6.7	46.7	26.6	0.6
Biuret	23.3	4.9	40.7	31.1	0.8
Meglumine	43.5	7.8	7.3	41.4	5.7



## Nitrogen in of fuels (dry %-wt)

Fossil fuels		Biomasses & waste - derived fuels	
Coal	0.5 – 3	Wood	0.1 – 0.5
		Bark	~ 0.5
Oil	< 1	Straw	0.5 – 1
Natural gas	0.5 – 20		
Light fuel oil	~ 0.2	Sewage sludge	~ 1
Heavy fuel oil	~ 0.5	Car tyre scrap	~ 0.3
		Municipal solid waste (MSW)	1 – 5
Peat	1 – 2	Refuse derived fuel (RDF)	~ 1
		Packaging derived fuel (PDF)	~ 1
Petroleum coke	~ 3	Auto shredder residue (ASR)	~ 0.5
		Leather waste	~ 12
Orimulsion™	~ 4	Black liquor solids	0.1 - 0.2



Fuel	New / Existing*	Plant size (MW <sub>th</sub> )	Emission standard (mg/m <sup>3</sup> <sub>STP</sub> dry)	Comments
Solid**	Existing	50 - 500	600 @ 6% O <sub>2</sub>	
“	“	> 500	500 @ 6% O <sub>2</sub>	Until 1.1.2016; if after 1.1.2008 < 2000 h/y then 600 @ 6% O <sub>2</sub>
“	“	> 500	200 @ 6% O <sub>2</sub>	After 1.1.2016; if < 1500 h/y then 450 @ 6% O <sub>2</sub>
Solid, general	New	50 - 100	400 @ 6% O <sub>2</sub>	
“	“	100 – 300	200 @ 6% O <sub>2</sub>	“Outermost regions” 300 @ 6% O <sub>2</sub>
“	“	> 300	200 @ 6% O <sub>2</sub>	
Solid, biomass	New	50 - 100	400 @ 6% O <sub>2</sub>	
“	“	100 – 300	200 @ 6% O <sub>2</sub>	
“	“	> 300	200 @ 6% O <sub>2</sub>	

\* Existing = plant existing on Nov. 27, 2002 ; or license for new plant requested before that date and plant entering operation before Nov. 27, 2003

\*\* Plants that operated during year 2000 on solid fuels with a volatile content less than 10 %-wt follow a limit of 1200 mg/m<sup>3</sup><sub>STP</sub> dry @ 6% O<sub>2</sub> until 1.1.2018

\*\*\* Applies only to > 70 % load and > 500 h/y operation. Limit is 75 mg/m<sup>3</sup><sub>STP</sub> dry @ 15 % O<sub>2</sub> for CHP plants > 75 % overall efficiency; combined cycle plants > 55 % electrical efficiency, or mechanical drives. Other, single cycle gas turbines, with efficiency  $\eta > 35$  % follow the limit value  $50 \times \eta / 35$  mg/m<sup>3</sup><sub>STP</sub> dry @ 15 % O<sub>2</sub>

**NO<sub>x</sub> (NO<sub>2</sub>)**  
**emission**  
**standards**  
**for EU**

**Solid Fuels**  
**(directive**  
**2001/80/EC)**





Fuel	New / Existing*	Plant size (MW <sub>th</sub> )	Emission standard (mg/m <sup>3</sup> <sub>STP</sub> dry)	Comments
Liquid	Existing	50 - 500	450 @ 3% O <sub>2</sub>	
“	“	> 500	400 @ 3% O <sub>2</sub>	
Liquid	New	50 – 100	400 @ 3% O <sub>2</sub>	
“	“	100 – 300	200 @ 3% O <sub>2</sub>	“Outermost regions” 300 @ 6% O <sub>2</sub>
“	“	> 300	200 @ 3% O <sub>2</sub>	
Liquid	New	> 50	120 @ 15 % O <sub>2</sub>	Gas turbines ***
Gas	Existing	50 - 500	300 @ 3% O <sub>2</sub>	
“	“	> 500	200 @ 3% O <sub>2</sub>	
Gas, natural	New	50 – 300	150 @ 3% O <sub>2</sub>	
“	“	> 300	100 @ 3% O <sub>2</sub>	
Gas, other	New	50 – 300	200 @ 3% O <sub>2</sub>	
“	“	> 300	200 @ 3% O <sub>2</sub>	
Natural gas	New	> 50	50 @ 15 % O <sub>2</sub>	Gas turbines ***
Other gas	New	> 50	120 @ 15 % O <sub>2</sub>	Gas turbines ***

- \* Existing = plant existing on Nov. 27, 2002 ; or license for new plant requested before that date and plant entering operation before Nov. 27, 2003
- \*\* Plants that operated during year 2000 on solid fuels with a volatile content less than 10 %-wt follow a limit of 1200 mg/m<sup>3</sup><sub>STP</sub> dry @ 6% O<sub>2</sub> until 1.1.2018
- \*\*\* Applies only to > 70 % load and > 500 h/y operation. Limit is 75 mg/m<sup>3</sup><sub>STP</sub> dry @ 15 % O<sub>2</sub> for CHP plants > 75 % overall efficiency; combined cycle plants > 55 % electrical efficiency, or mechanical drives. Other, single cycle gas turbines, with efficiency  $\eta > 35 \%$  follow the limit value  $50 \times \eta / 35$  mg/m<sup>3</sup><sub>STP</sub> dry @ 15 % O<sub>2</sub>

## NO<sub>x</sub> (NO<sub>2</sub>) emission standards for EU

## Liquid and Gaseous Fuels

(directive  
2001/80/EC)



Type of plant	Plant	Emission standard (mg/m <sup>3</sup> <sub>STP</sub> dry)	Comments
Waste incineration	< 6 t /h	200 @ 10 % O <sub>2</sub> *	Daily average
“	> 6 t /h	400 @ 10 % O <sub>2</sub> *	Daily average
Cement, incl. co-firing	All	800 / 500 @ 10 % O <sub>2</sub>	Existing / new **
Waste co-firing ***	50 – 100 MW <sub>th</sub>	C <sub>process</sub> 400 @ 6 % O <sub>2</sub>	Solid fuel
“	“	C <sub>process</sub> 350 @ 6 % O <sub>2</sub>	Biomass
“	“	C <sub>process</sub> 400 @ 3 % O <sub>2</sub>	Liquid fuel
“	100 – 300 MW <sub>th</sub>	C <sub>process</sub> 300 @ 6 % O <sub>2</sub>	Solid fuel
“	“	C <sub>process</sub> 300 @ 6 % O <sub>2</sub>	Biomass
“	“	C <sub>process</sub> 400 @ 3 % O <sub>2</sub>	Liquid fuel
“	> 300 MW <sub>th</sub>	C <sub>process</sub> 200 @ 6 % O <sub>2</sub>	Solid fuel
“	“	C <sub>process</sub> 300 @ 6 % O <sub>2</sub>	Biomass
“	“	C <sub>process</sub> 400 @ 3 % O <sub>2</sub>	Liquid fuel

\* Various exceptions until 1.1.2008 or 1.1.2010, and until 1.1.2007 these regulations do not apply to hazardous waste incineration

\*\* Existing = plant existing on Dec. 28, 2002; or license for new plant requested before that date and plant entering operation on Dec. 28, 2003 or Dec. 28, 2004. Until 1.1.2008 special regulation 1200 mg/m<sup>3</sup><sub>STP</sub> dry @ 10 % O<sub>2</sub> for existing wet kilns and small kilns co-firing less than 3 t waste /h.

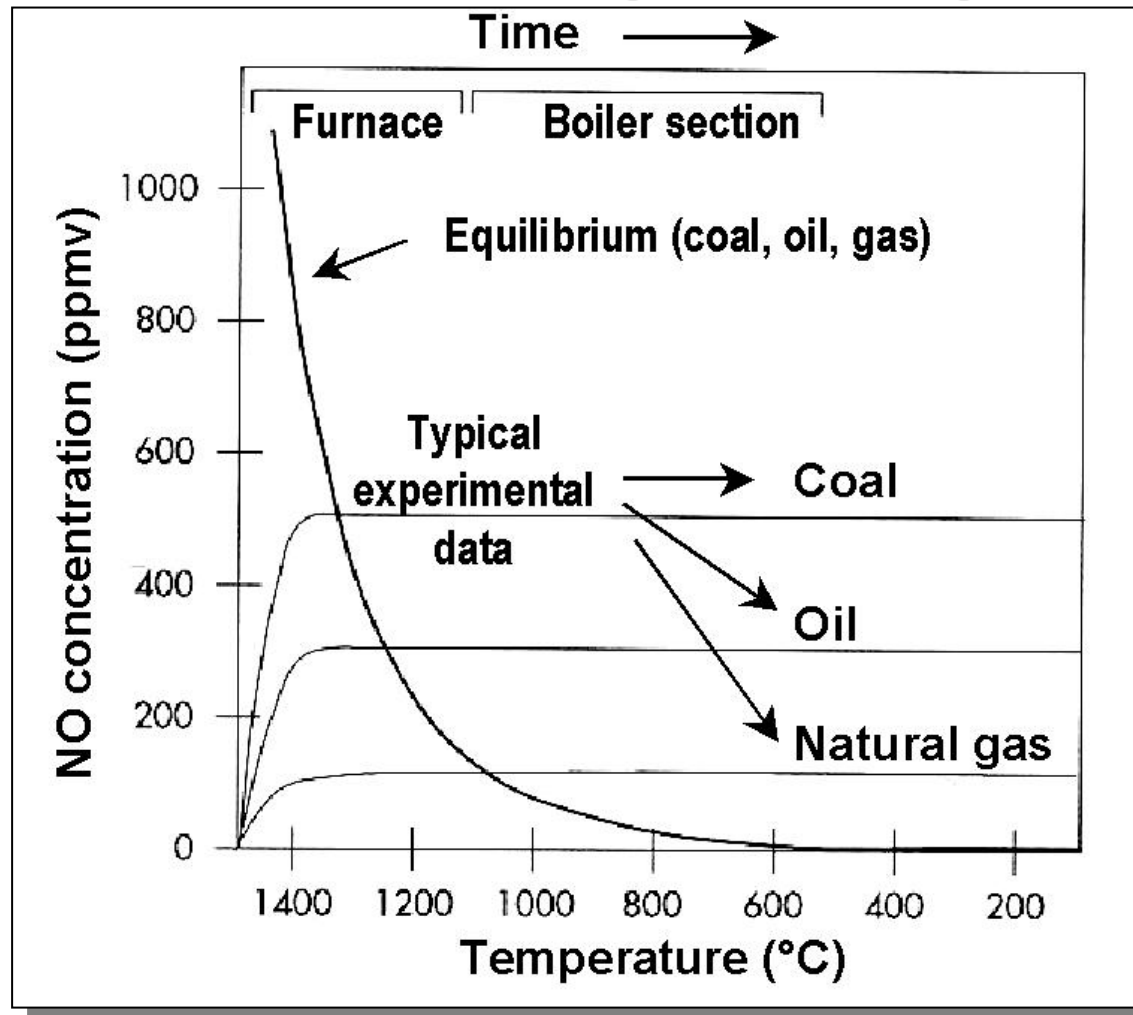
\*\*\* Various exceptions until 1.1.2008 for existing fluidised beds 100 – 300 MW<sub>th</sub> that burn solid fuels or biomass provided that C<sub>process</sub> < 350 mg/m<sup>3</sup><sub>STP</sub> dry @ 6 % O<sub>2</sub>. Until 1.1.2007 these regulations do not apply to hazardous waste incineration

# NO<sub>x</sub> (NO<sub>2</sub>) emission standards for waste (co-) firing and cement plants for EU (directive 2000/76/EC)

$$C_{\text{co-firing}} = (V_{\text{waste}} \cdot C_{\text{waste}} + V_{\text{process}} \cdot C_{\text{process}}) / (V_{\text{waste}} + V_{\text{process}}), V = \text{exhaust volume}$$

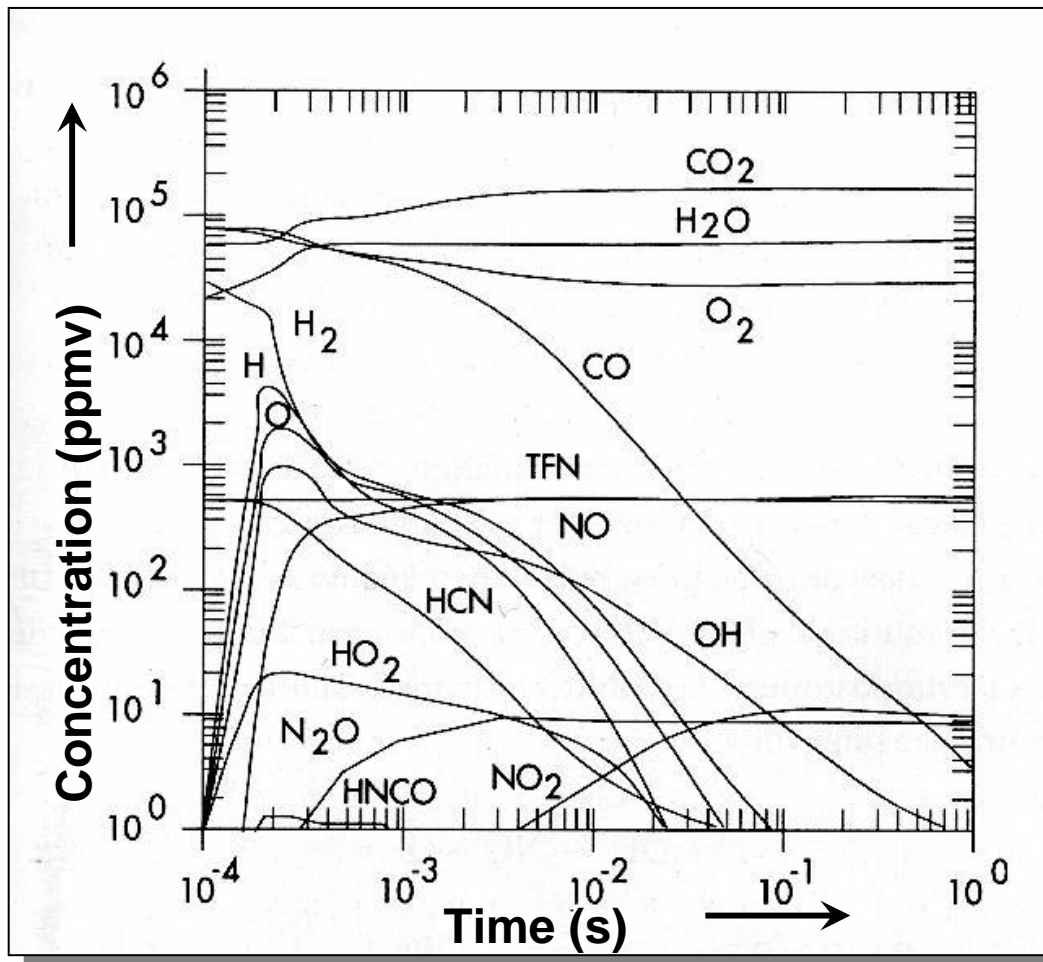


# NO formation in pulverised coal, oil and natural gas firing



Thermodynamics  
*versus*  
measurements

# Kinetic modelling of coal pyrolysis gas combustion



Combustion in  
plug flow reactor (PFR).  
850°C, 1 bar.

Initial gas (%-vol):  
8% CO, 3% H<sub>2</sub>, 2% H<sub>2</sub>O  
0.05% HCN, 8% O<sub>2</sub>, 73% N<sub>2</sub>

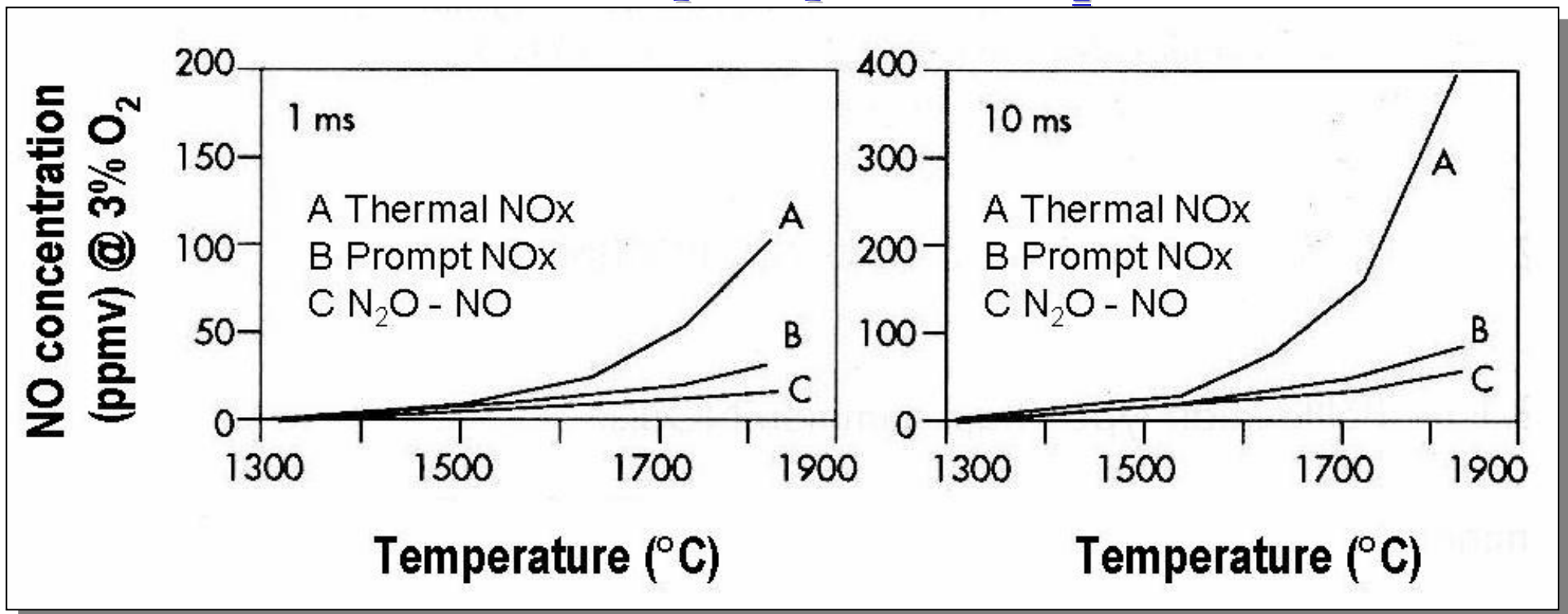


## NO Formation from $\text{N}_2$ Fixation: $\text{N}_2 \rightarrow \text{NO}$

n:o	Reaction
1	Thermal NO $\text{N}_2 + \text{O} \rightarrow \text{NO} + \text{N}$ $\text{N} + \text{O}_2 \rightarrow \text{NO} + \text{O}$ $\text{N} + \text{OH} \rightarrow \text{NO} + \text{H}$
2	Prompt NO $\text{N}_2 + \text{CH} \rightarrow \text{HCN} + \text{N}$ $\text{HCN} \xrightarrow{+\text{O}} \text{NCO} \xrightarrow{+\text{H}} \text{NH} \xrightarrow{+\text{H}} \text{N} \xrightarrow{+\text{O}_2, +\text{OH}} \text{NO}$
3	Formation via $\text{N}_2\text{O}$ intermediate $\text{O} + \text{N}_2 + \text{M} \rightarrow \text{N}_2\text{O} + \text{M}$ $\text{N}_2\text{O} + \text{O} \rightarrow 2\text{NO}$



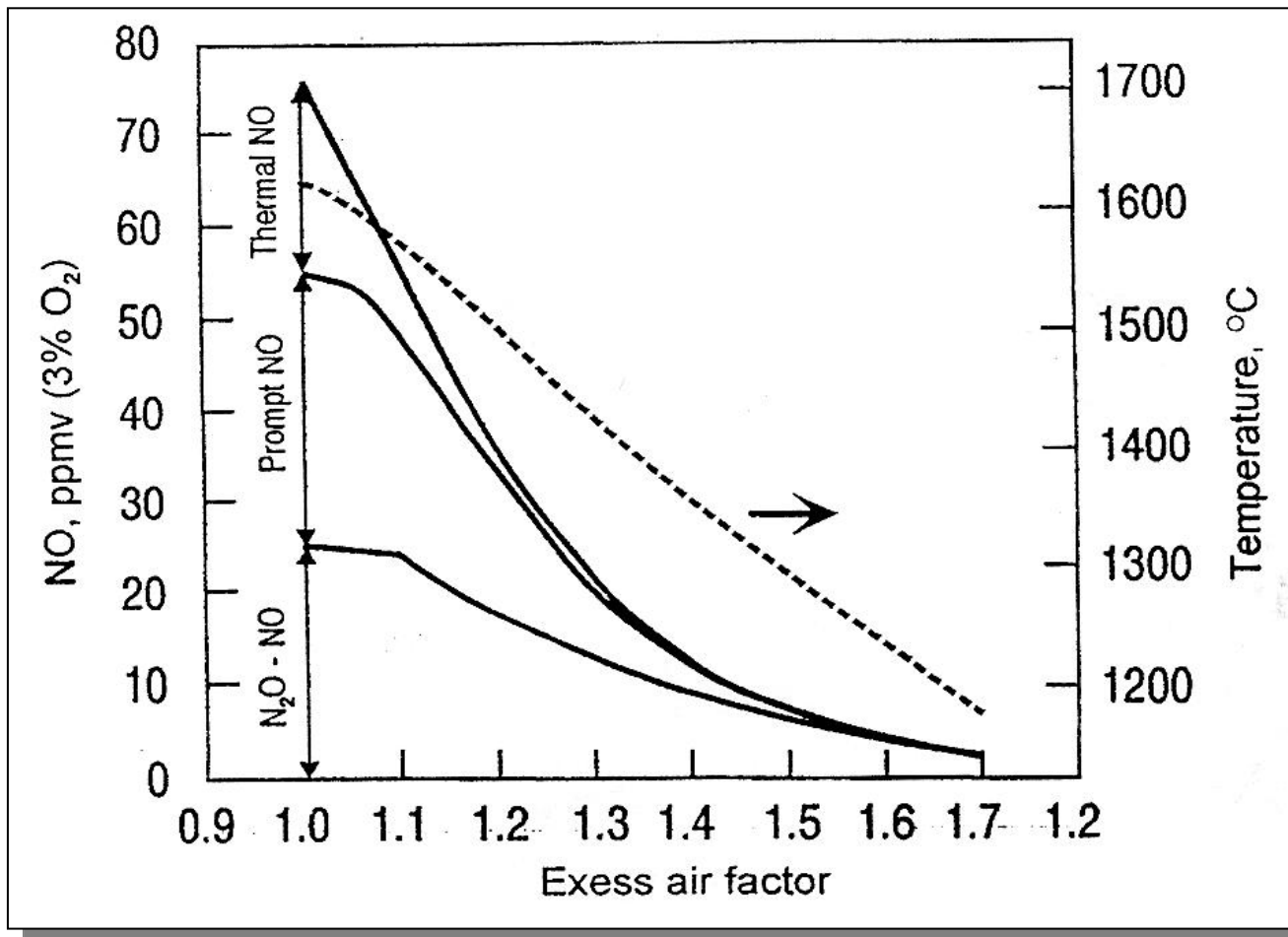
## Kinetic modelling of NO formation: thermal NO<sub>x</sub>, prompt NO<sub>x</sub>, N<sub>2</sub>O-NO



Methane combustion with air in a stirred reactor (CSTR), at 1 bar, air factor  $\lambda = 1.15$

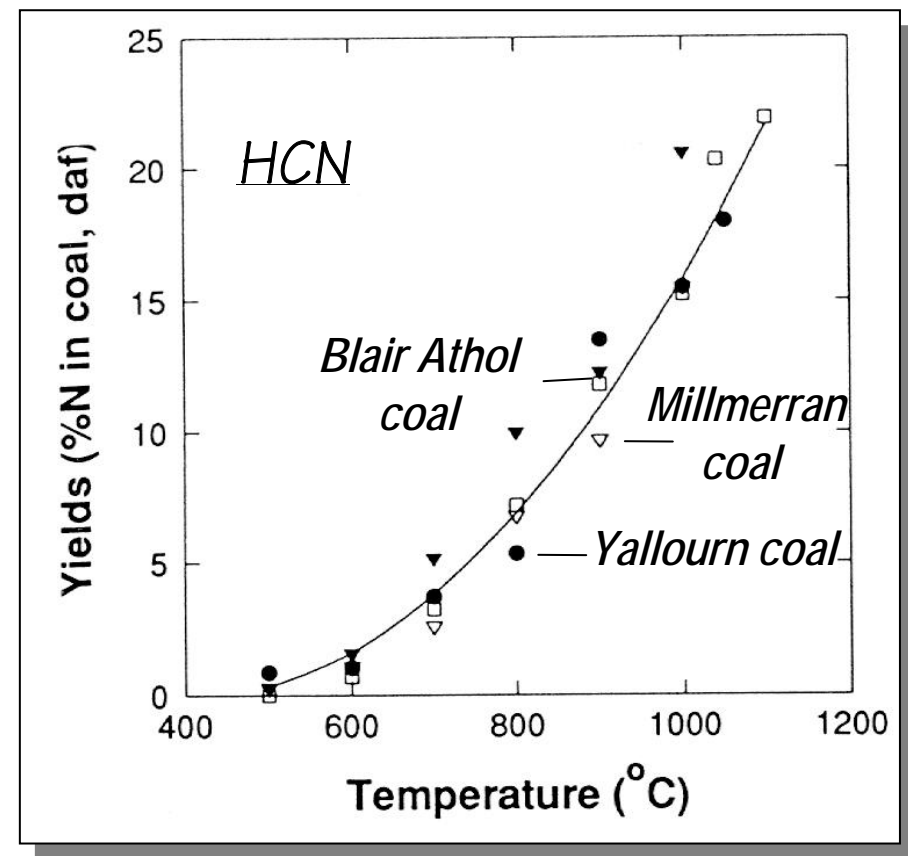
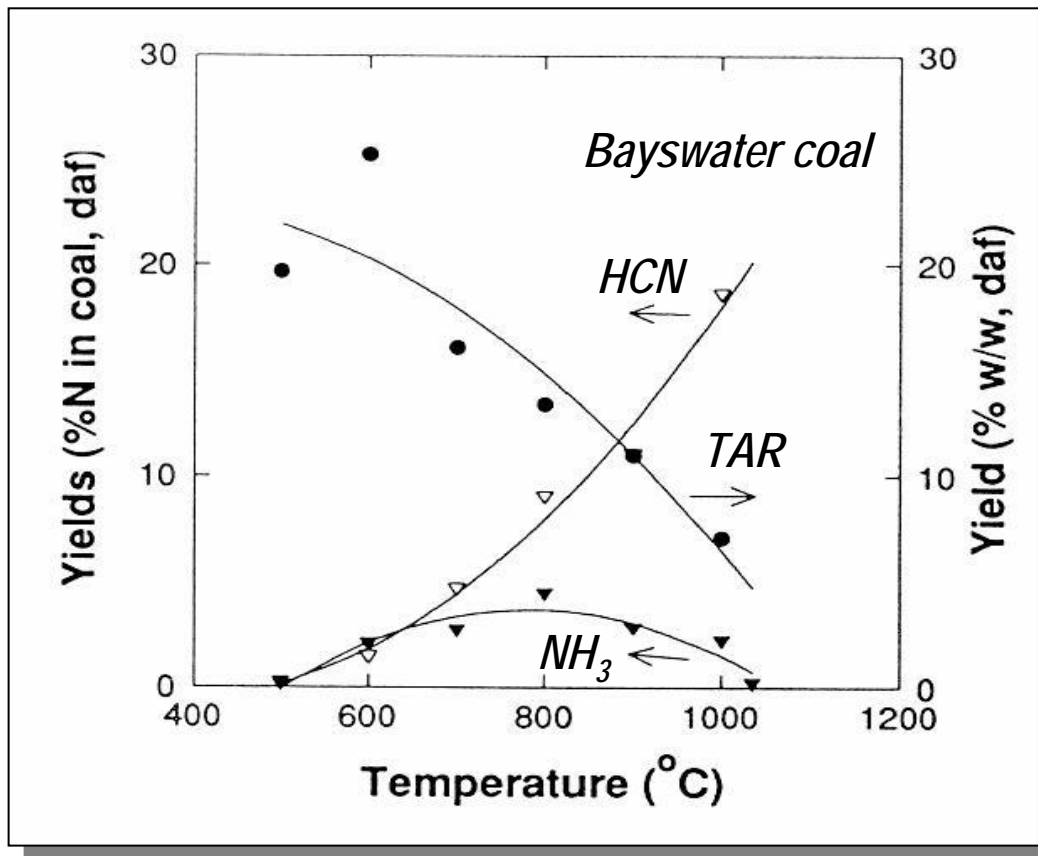


## NO formation mechanisms: effect of air factor, $\lambda$



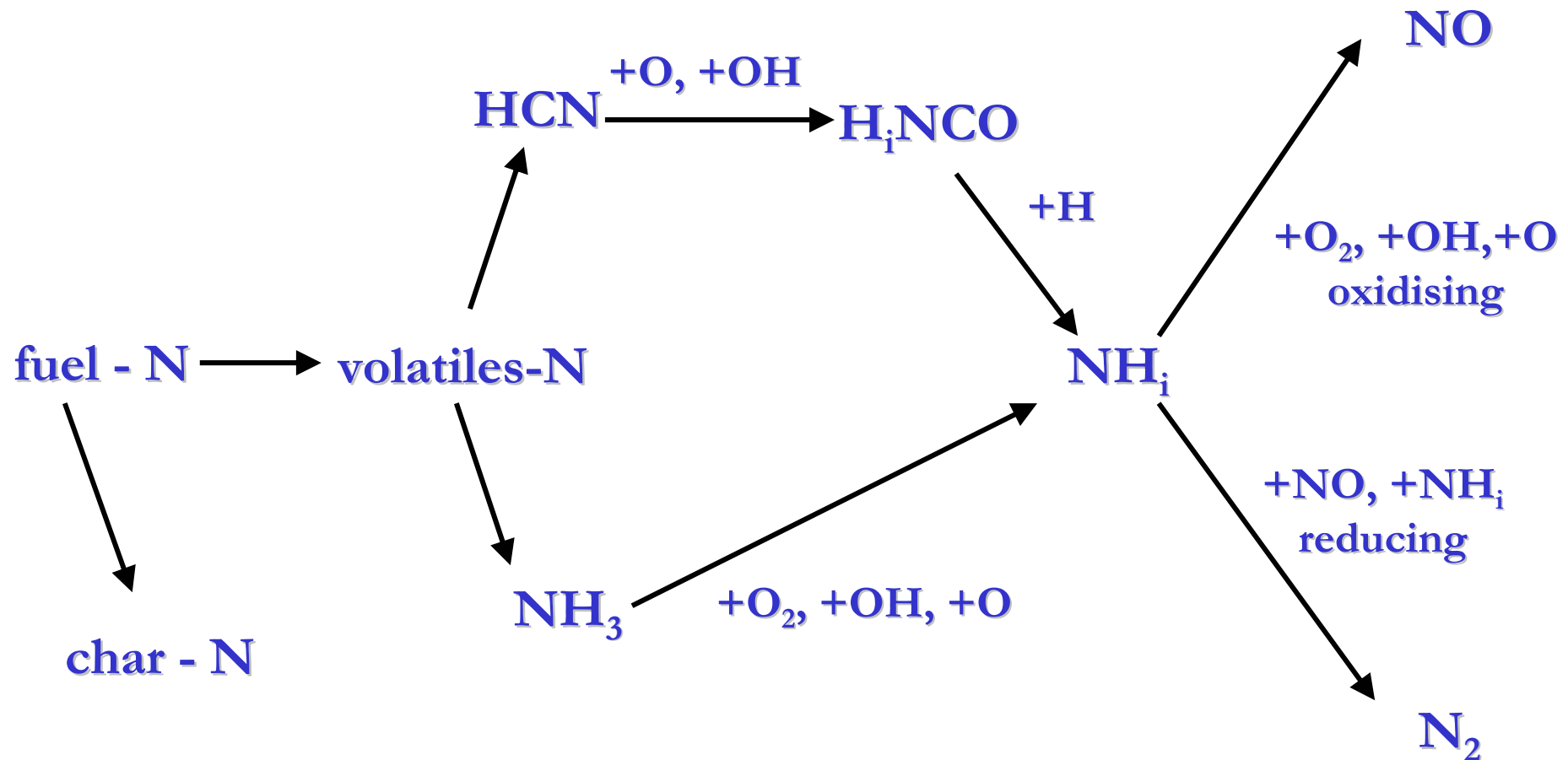
Methane combustion  
with air  
in a stirred reactor  
(CSTR),  
at 1 bar,  
residence time 4 ms.

# Release of Fuel-N during pyrolysis of Australian coal





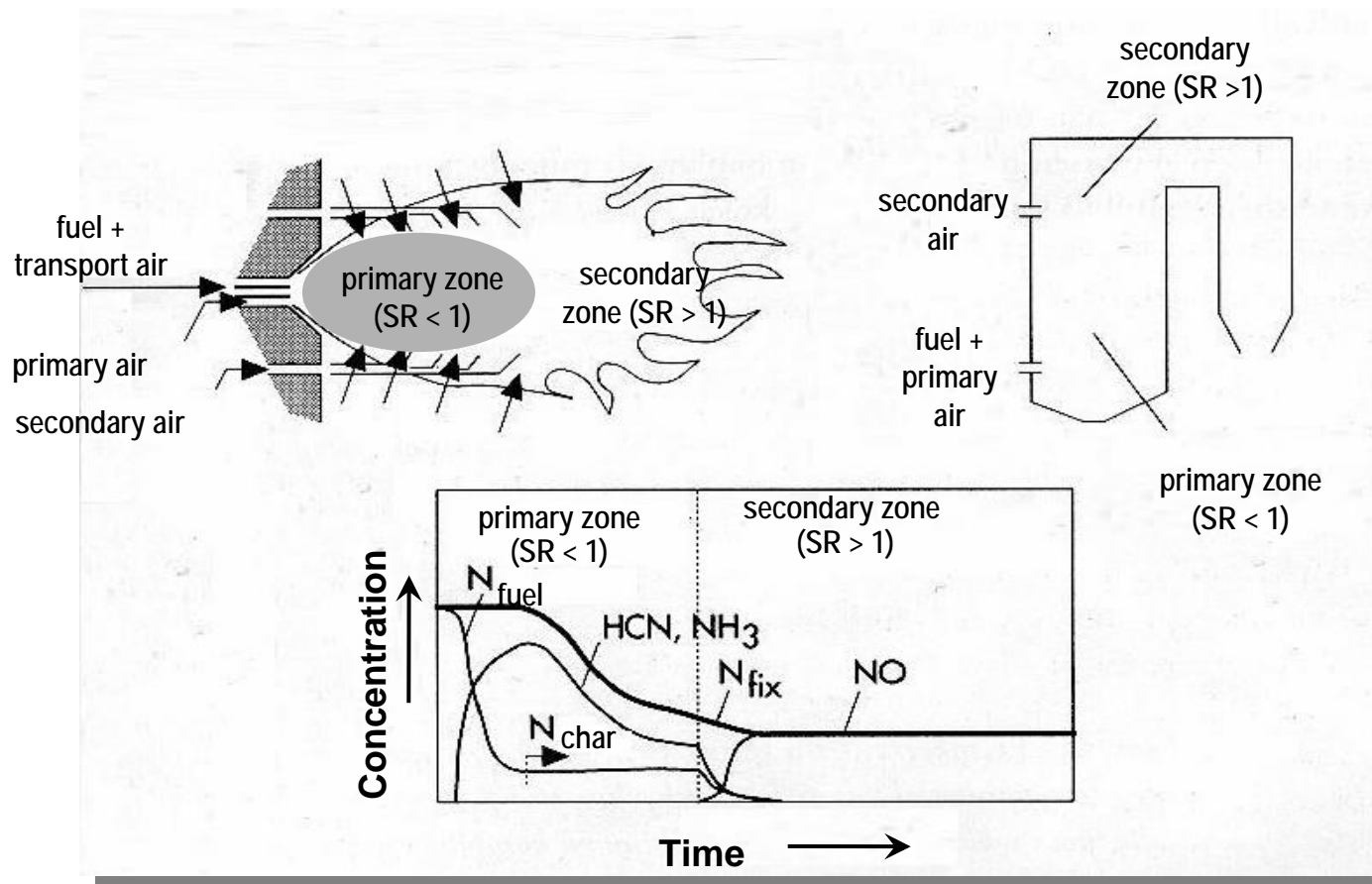
## Oxidation of volatile fuel-N compounds during burner combustion (simplified)



# Principle of air staging.

Assumed: char-N gives NO (40%) and N<sub>2</sub> (60%),

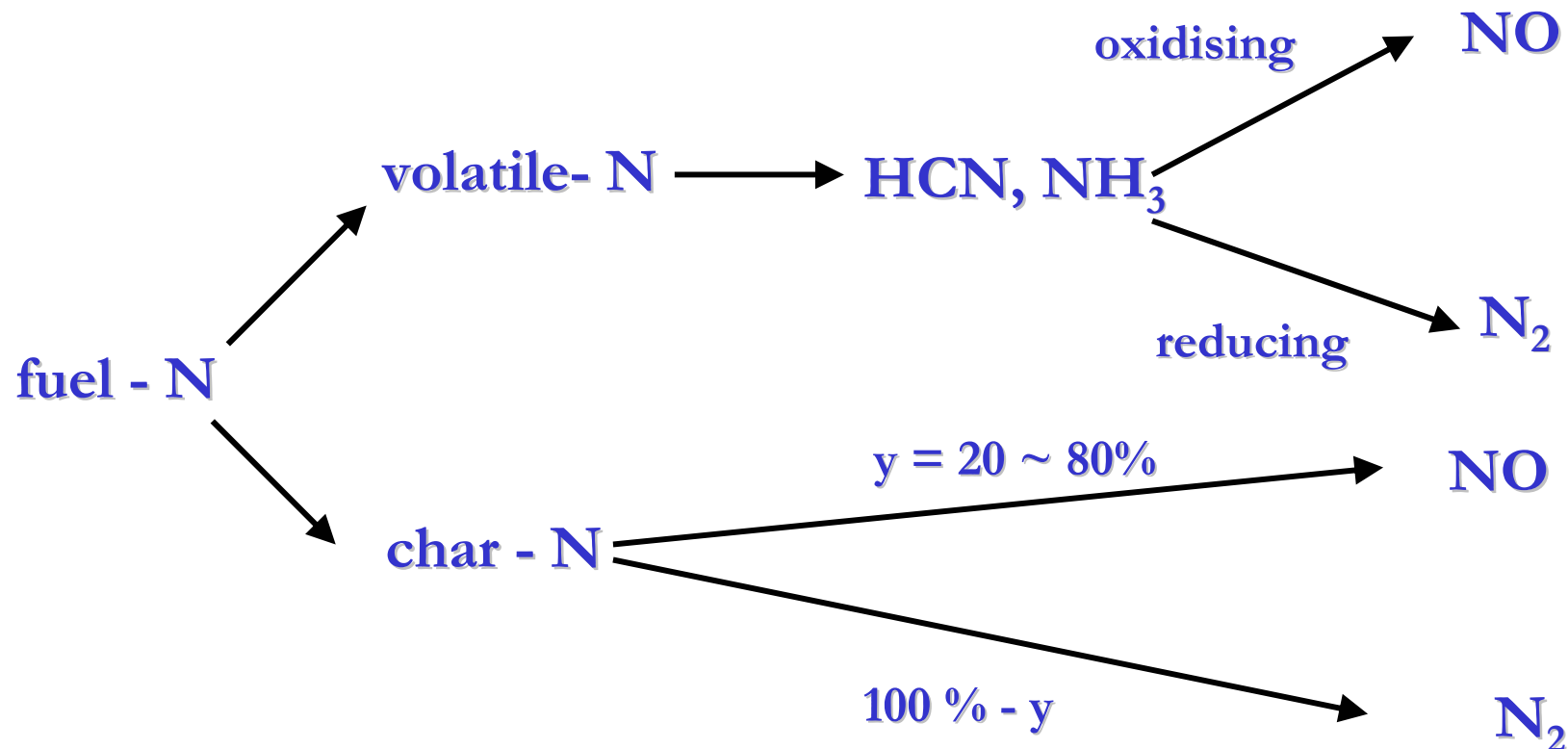
N<sub>fix</sub> = all nitrogen compound except N<sub>2</sub>



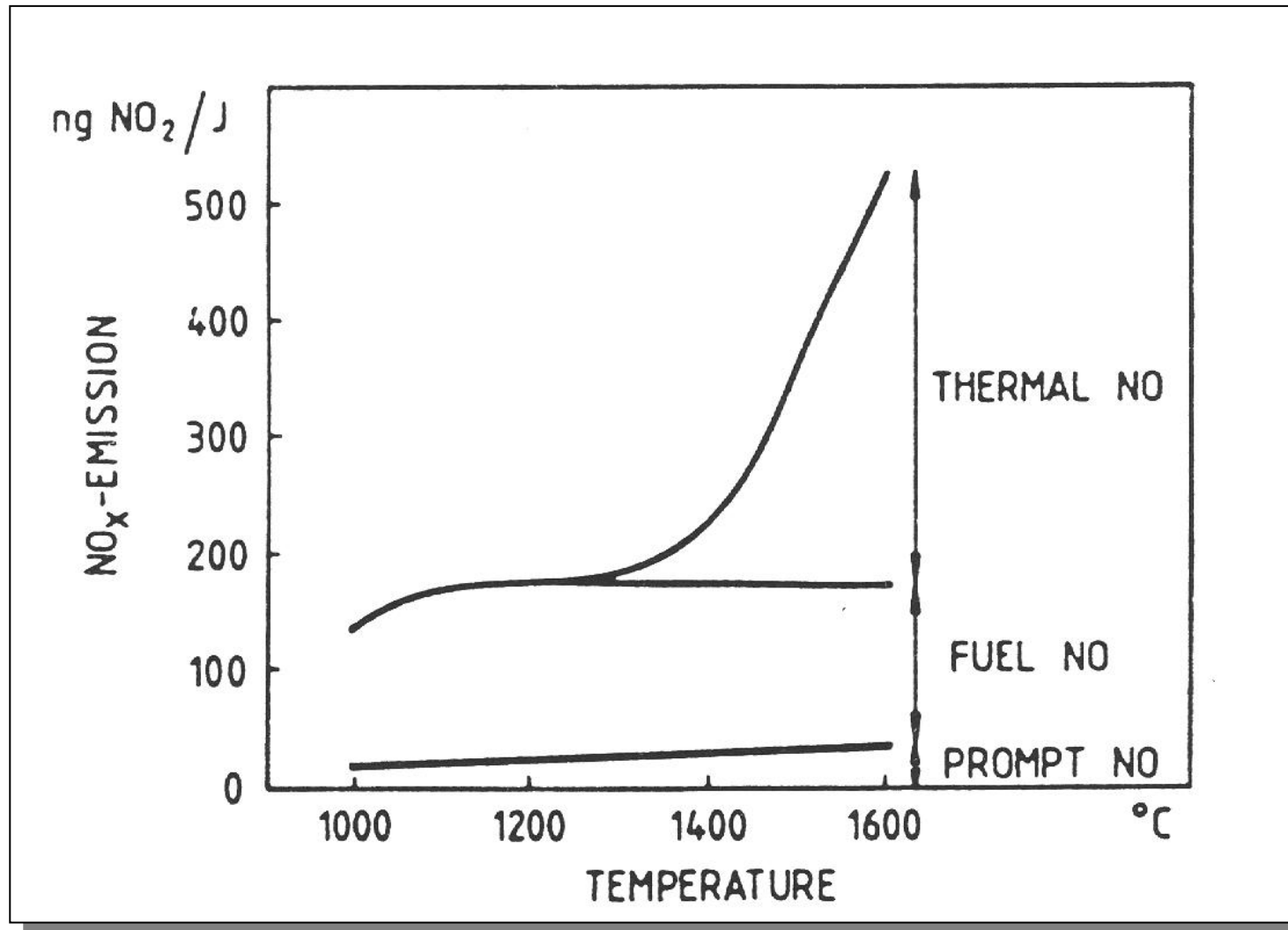




## Oxidation of fuel-N to NO and N<sub>2</sub> during burner combustion with significant char-N (simplified)



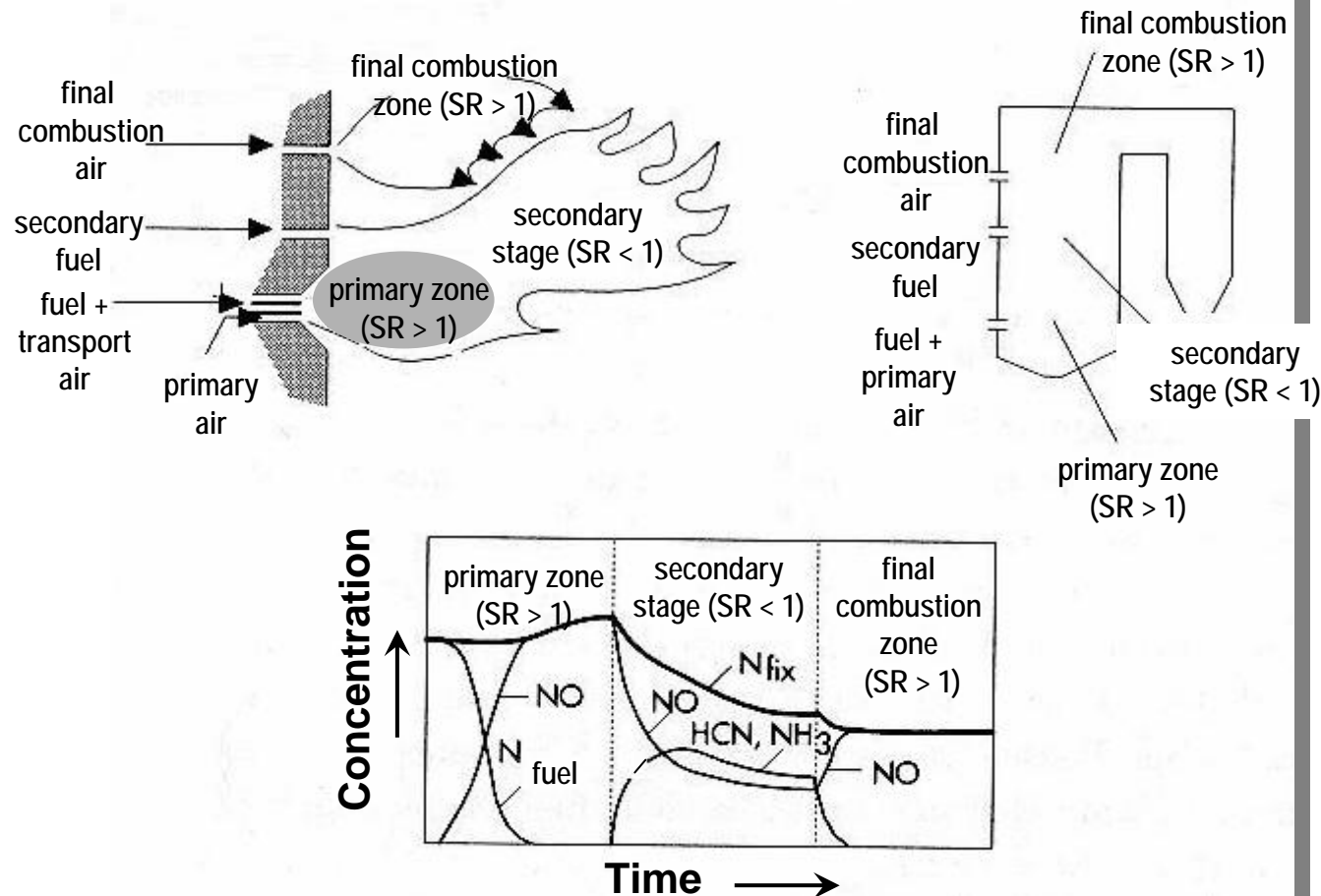
## Thermal NO<sub>x</sub>, prompt NO<sub>x</sub>, fuel NO<sub>x</sub>

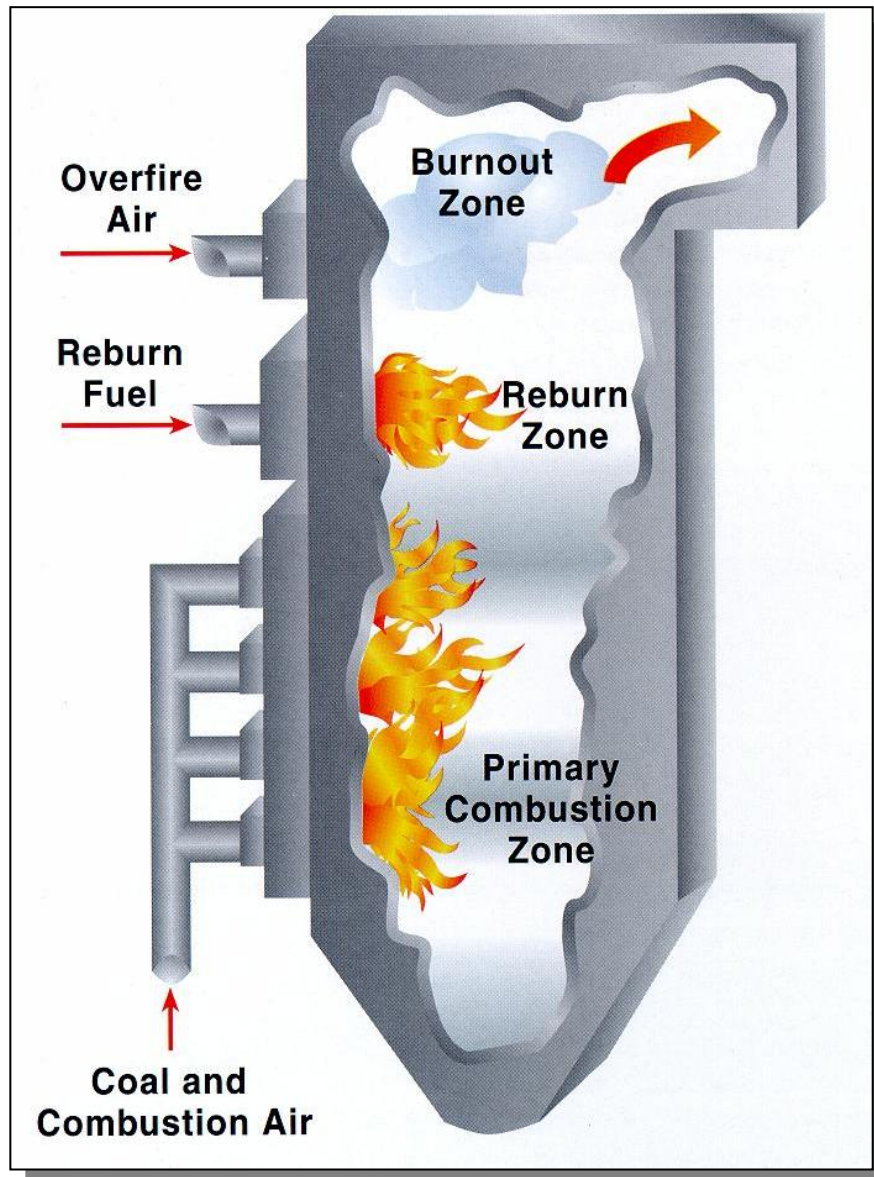


# Principle of fuel staging.

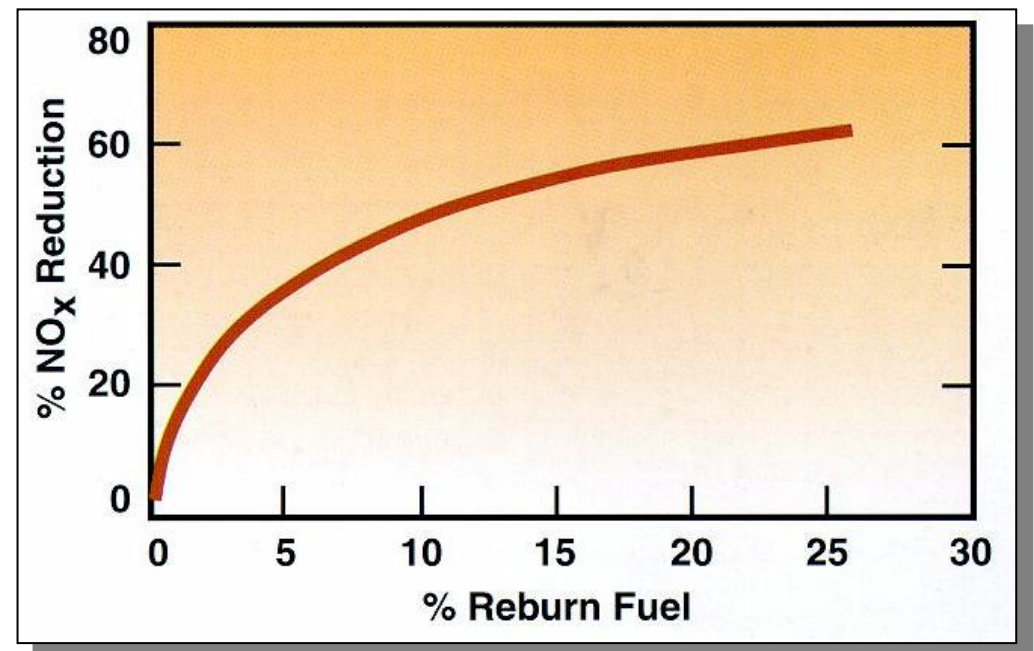
Assumed: fuel NO and thermal NO formed during primary stage,

$N_{fix}$  = all nitrogen compound except  $N_2$

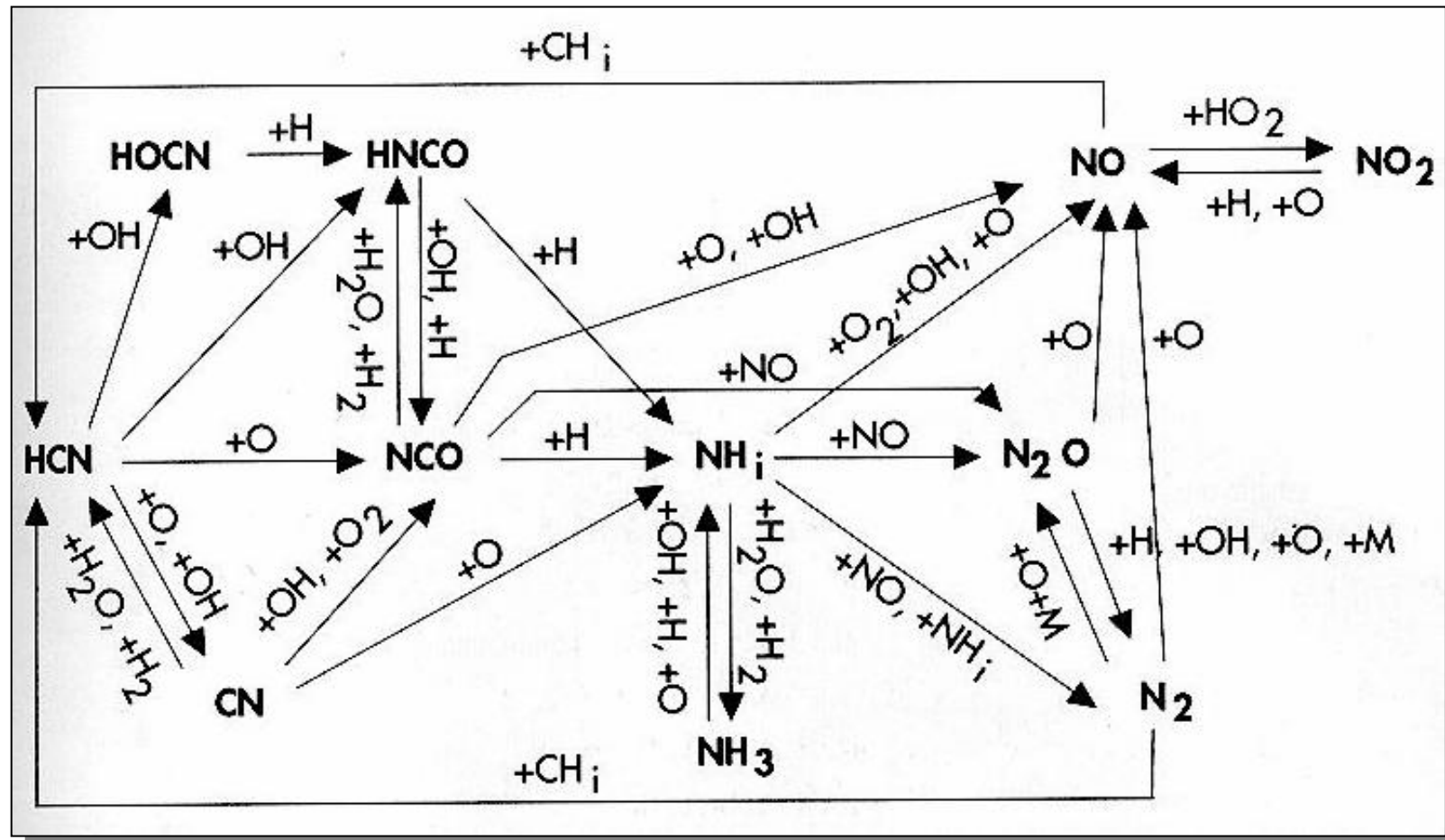




## Reburning technology



# Main NO<sub>x</sub> formation and decomposition reactions during burner combustion (summary)

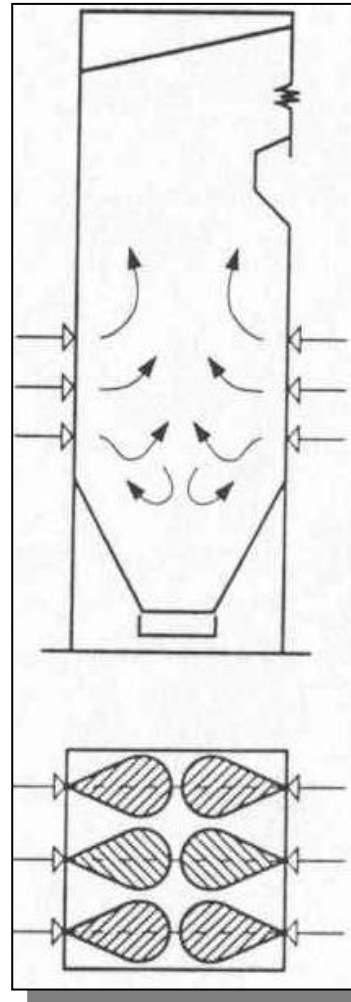
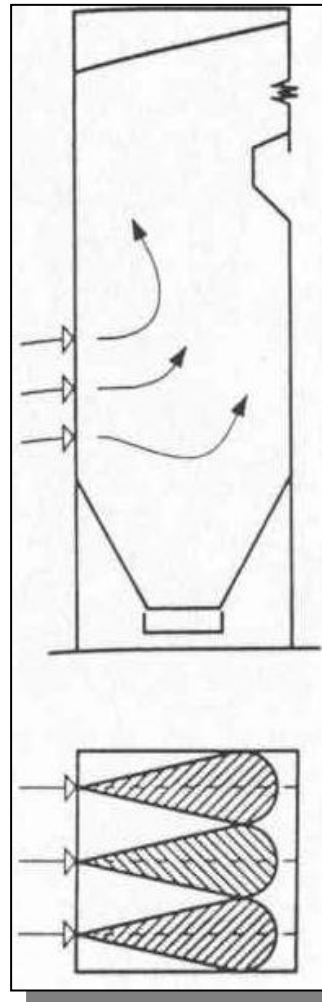




# Pulverised fuel combustion furnace types



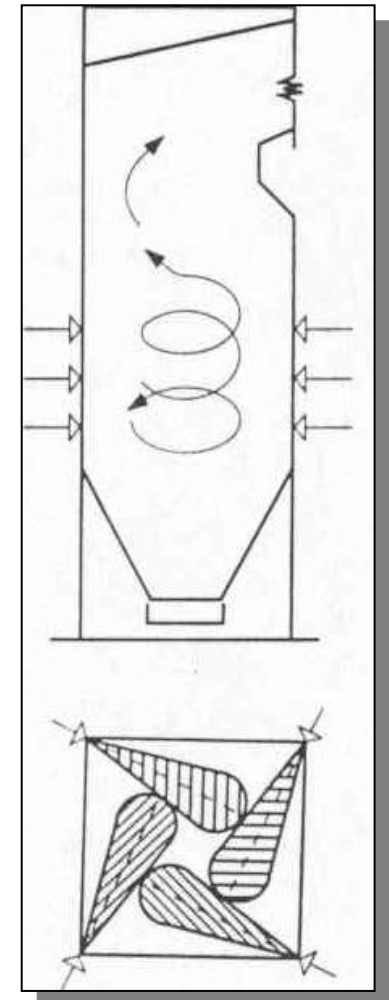
*A typical  
pulverised coal-firing  
flame*

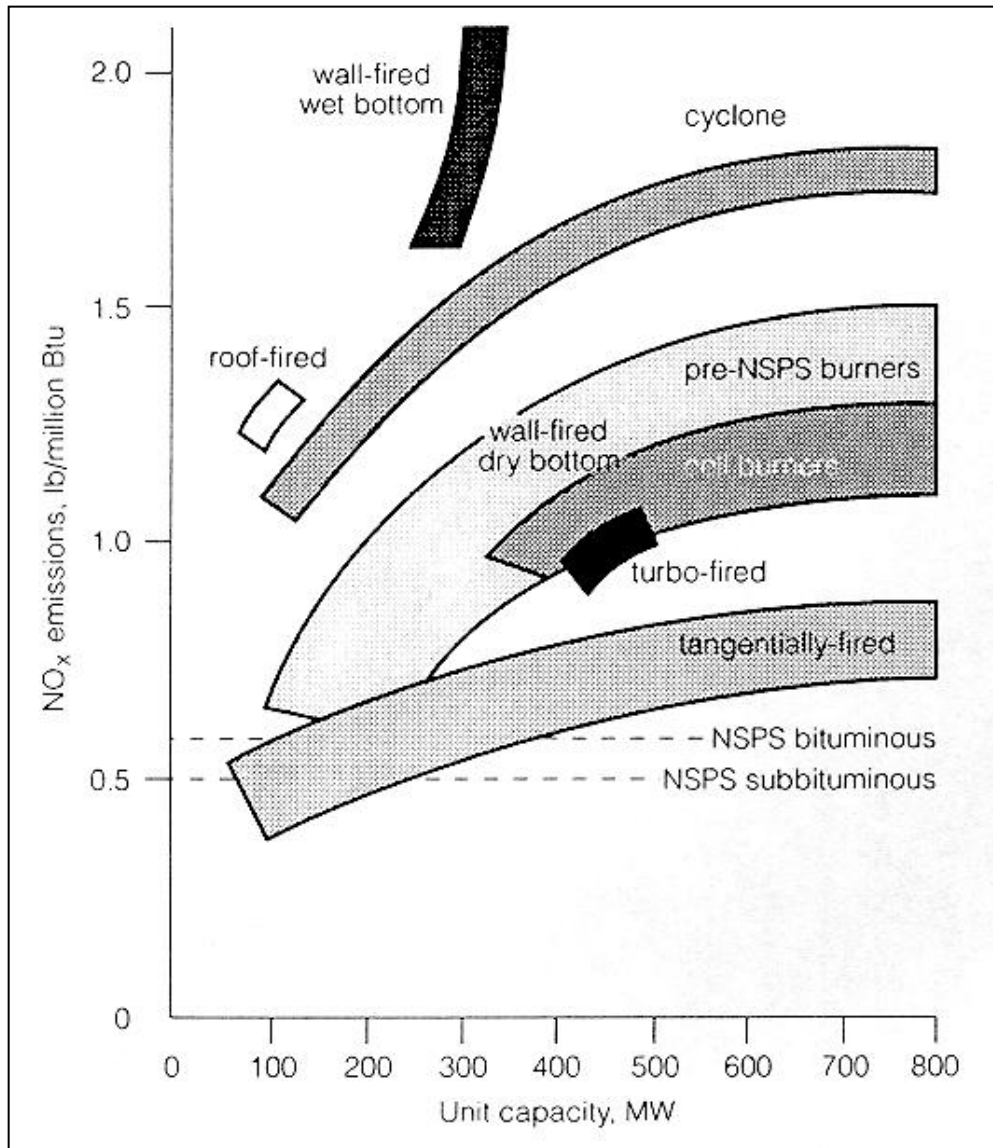


← ←  
**Front wall  
fired**

←  
**Opposed wall  
fired**

→  
**Tangential /  
corner  
fired**

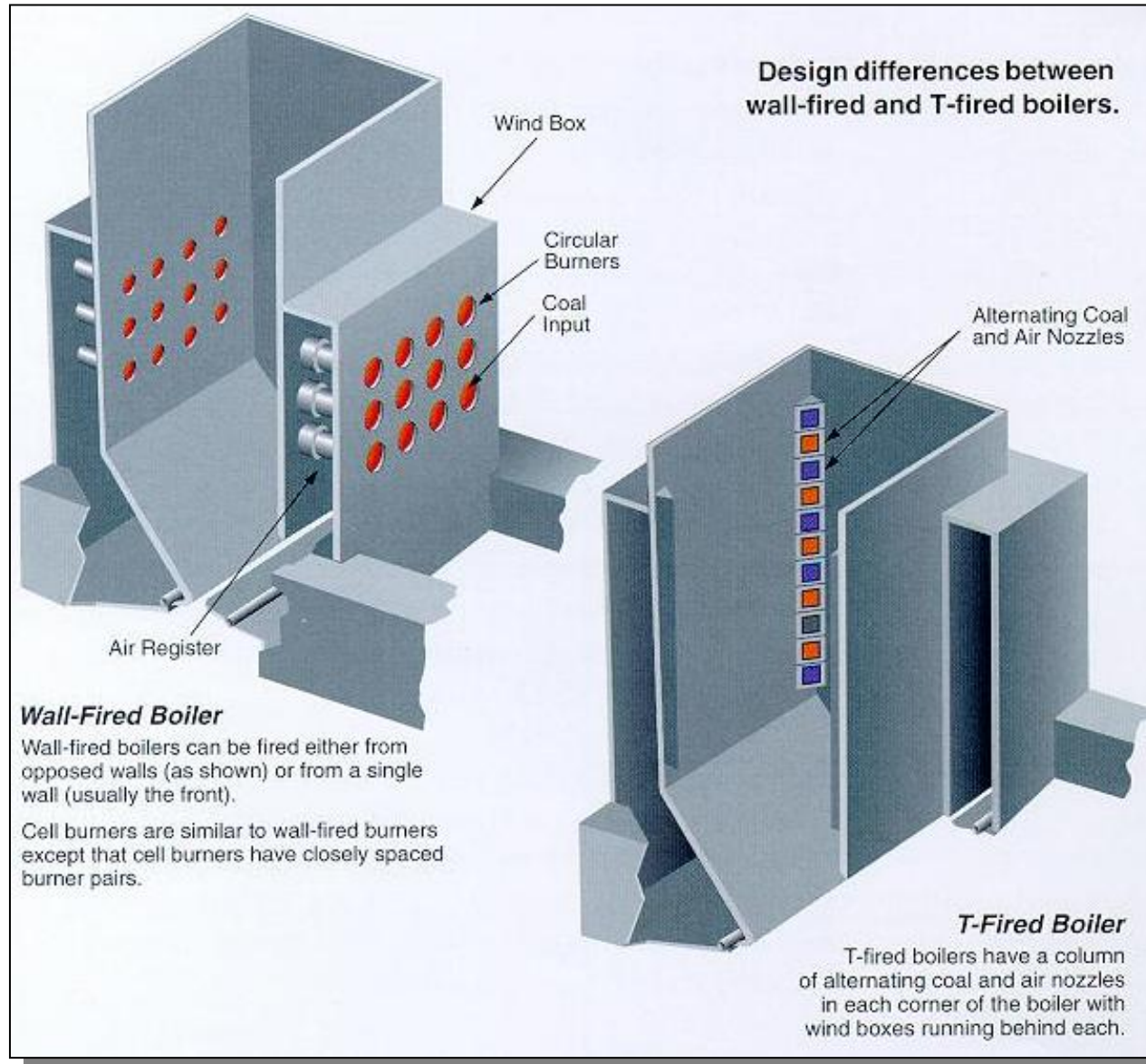




Typical NO<sub>x</sub>  
emissions for  
various types of  
coal-fired  
furnaces as  
function of unit  
size

Note : 1 lb/MBTU ~  
0.5 mg/GJ

*NSPS = New Source Performance Standard*



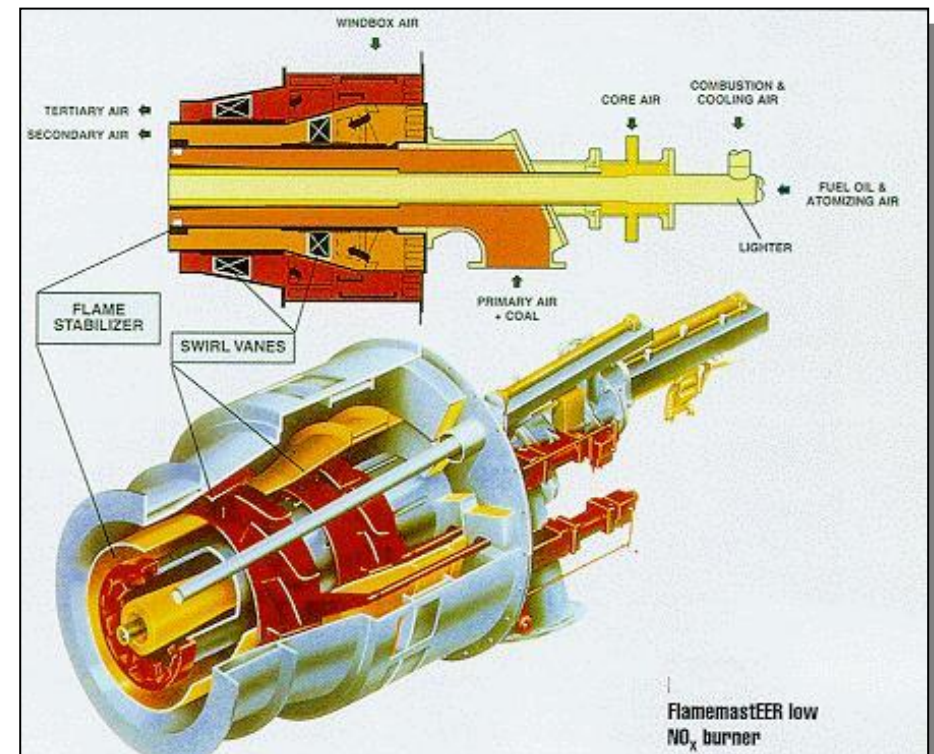
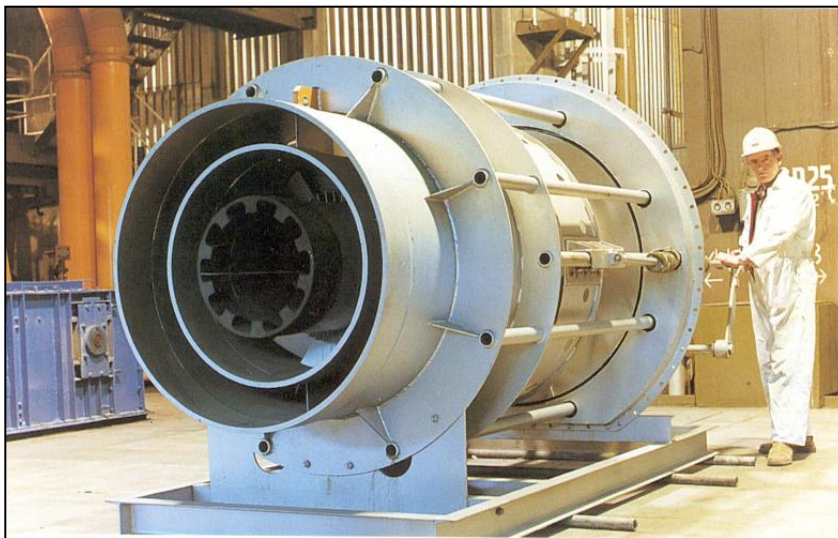
# Wall-fired burner combustion and tangential combustion (T-firing)



# Low-NO<sub>x</sub> burners for pulverised coal firing



Tip of low-NO<sub>x</sub> burner installed on Unit 4 at Arapahoe Station.



# IFRF flame type classification system

Reverse flow leads to rapid ignition close to the burner, resulting in NO reduction.  
Sufficient penetration and time in IRZ is crucial !!!!!

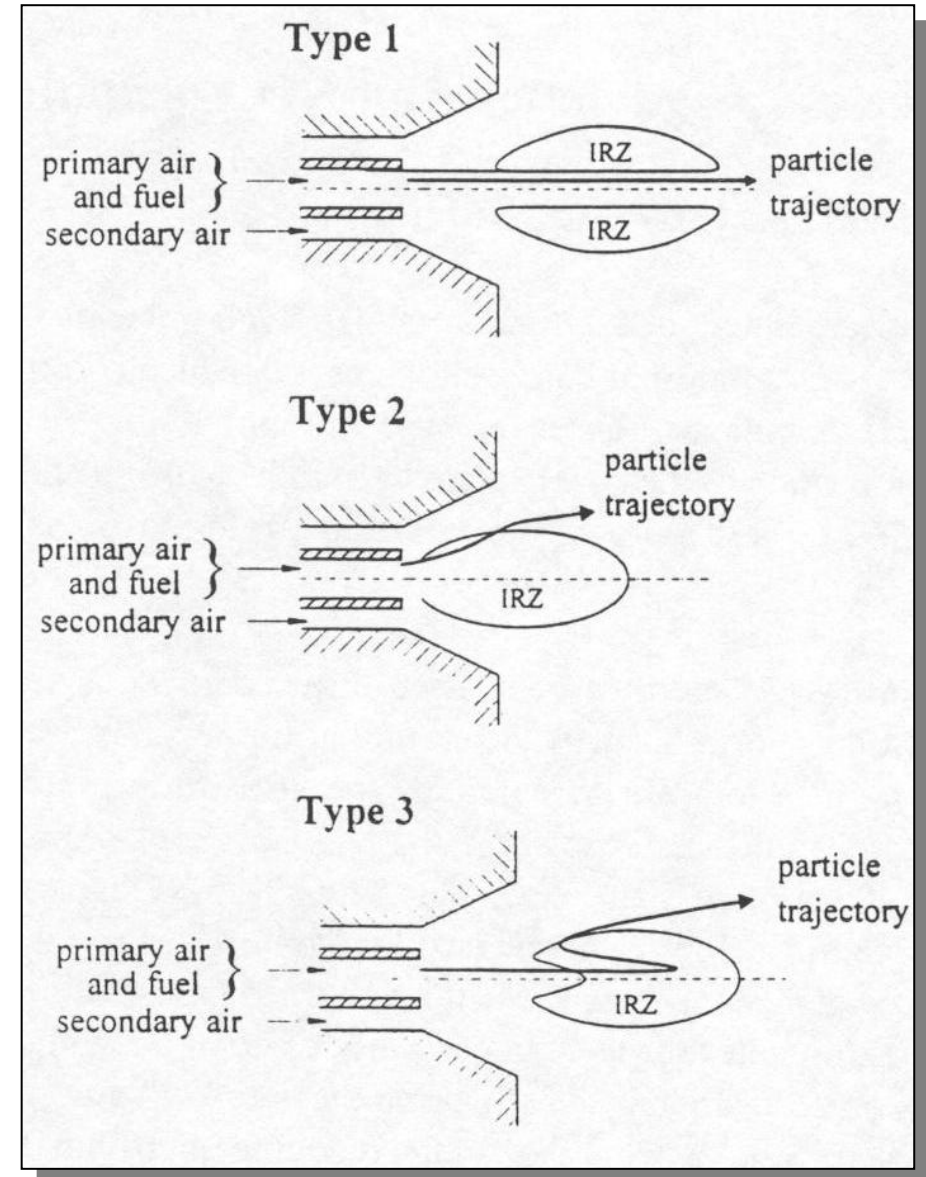
Stoichiometry in primary zone:

$\lambda \sim 0.6 \dots 0.7$  is optimal

$\lambda > 0.7$  gives more NO

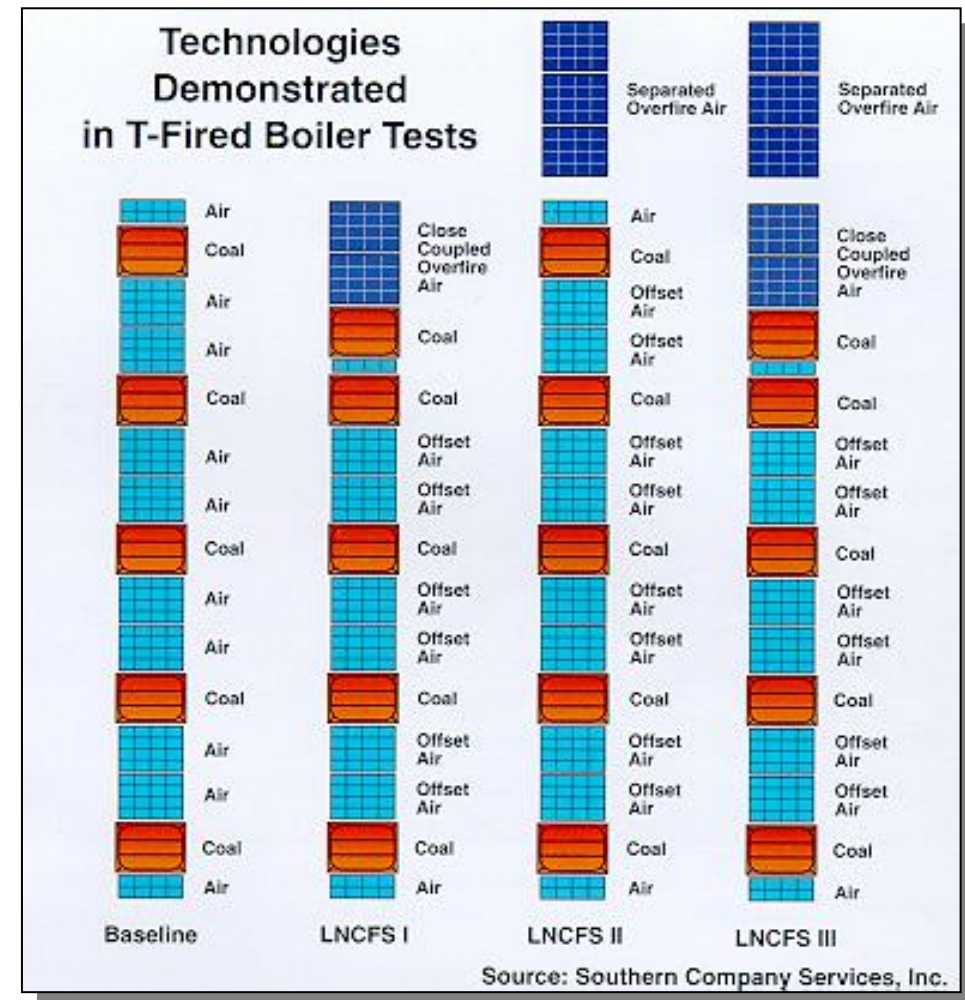
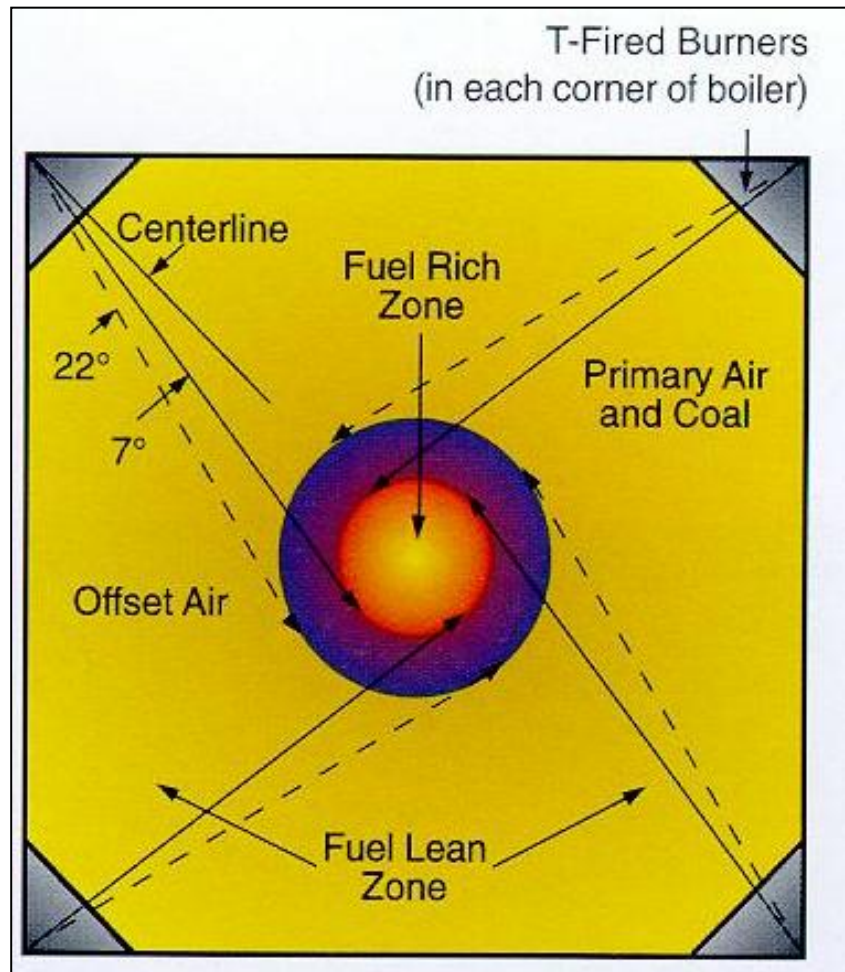
$\lambda < 0.6$  gives more  $\text{NH}_3$ ,  $\text{HCN}$ ,... giving more post-flame NO

Stoichiometry  $\downarrow$  then NO  $\downarrow$ ,  
but carbon-in-ash  $\uparrow$  and corrosion  $\uparrow$

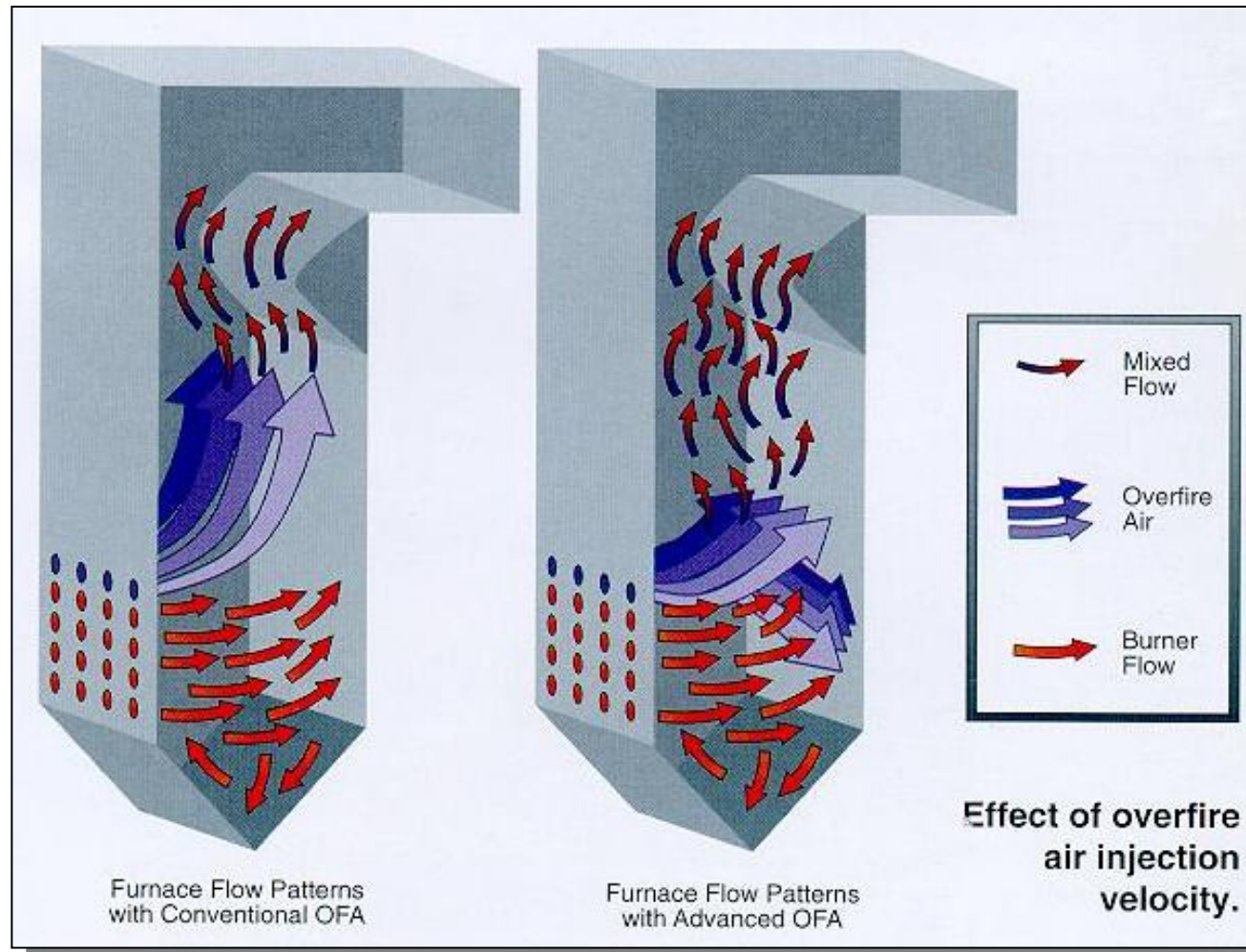




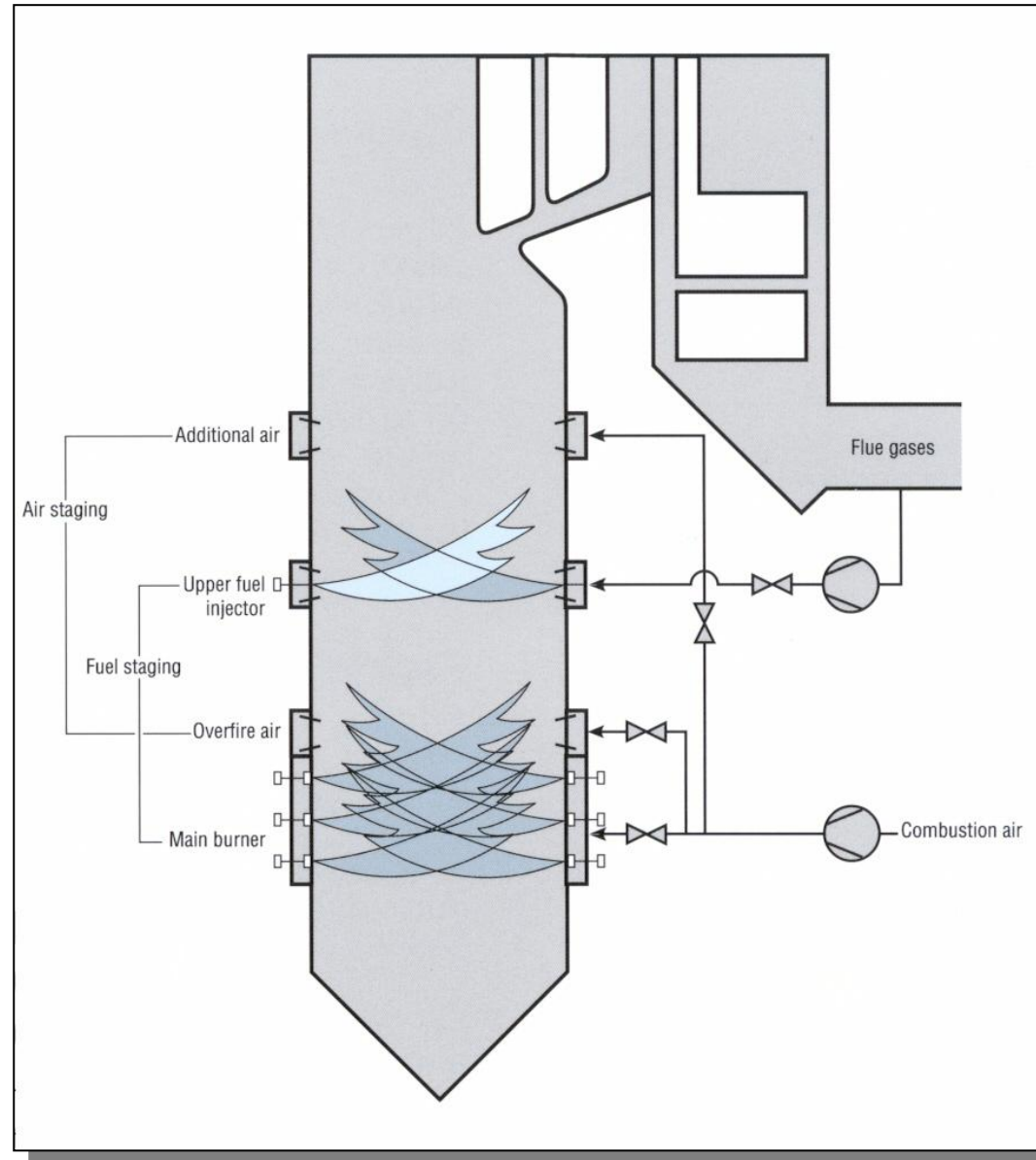
## Low-NO<sub>x</sub> concentric firing system (LCNFST<sup>TM</sup>)



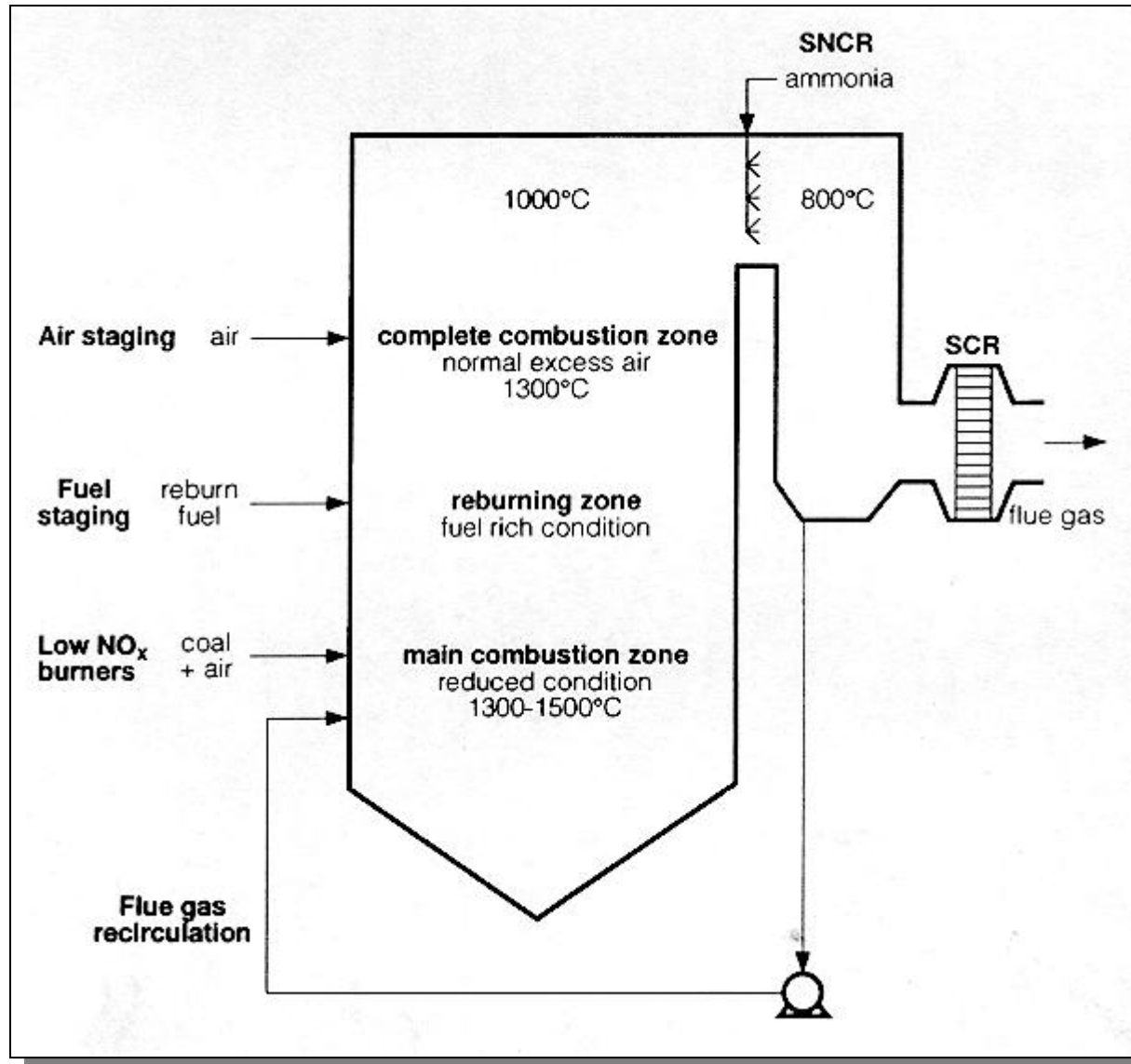
## Overfire air (OFA) and advanced OFA



# Air and fuel staging for NO<sub>x</sub> control







## Overview of Low- $\text{NO}_x$ technologies for burner combustion



## Overview of Low NO<sub>x</sub> technologies

	<b>Advantageous when</b>	<b>Problems</b>
<b>Low excess air</b>	When excess air is used	Fuel burnout decreases
<b>Air staging / over-fire air</b>	In principle always	Limited effect, increased risks for corrosion, fouling, slagging
<b>Low NO<sub>x</sub> burner <i>i.e.</i> in-flame staging</b>	In principle always	Fuel burn-out decreases, not a big problem, however
<b>Fuel staging <i>i.e.</i> reburning with coal, oil, natural gas</b>	In principle always, especially when the reburn fuel is also the start-up fuel	Capital cost of system modifications
<b>Flue gas recirculation</b>	High temperature oil- or gas-fired furnaces	Low efficiency if not combined with other method



## Relative effects of Low-NO<sub>x</sub> technologies

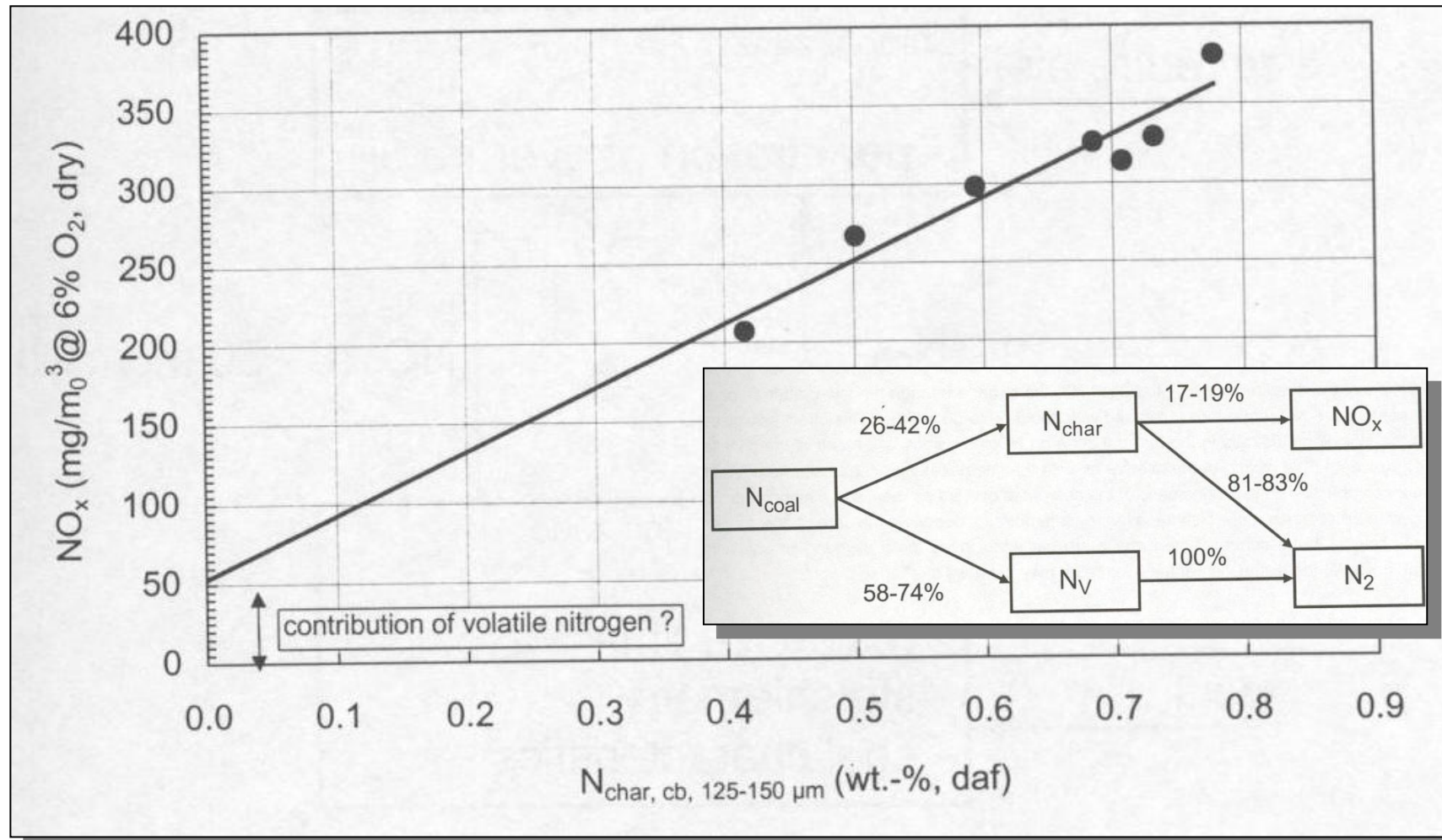
Measures	NO <sub>x</sub> emissions, ppmv (6%, O <sub>2</sub> )	NO <sub>x</sub> reduction, %
Base	550–800	–
Low excess air	450–650	15–20
Low excess air + over fire air	300–500	35–45
Low excess air + flue gas recirculation	350–550	30–35
Low excess air + over fire air + flue gas recirculation	200–400	50–60
Low excess air + over fire air + flue gas recirculation + low NO <sub>x</sub> burners	150–300	60–70



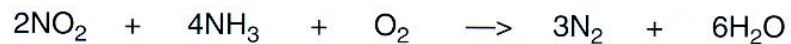
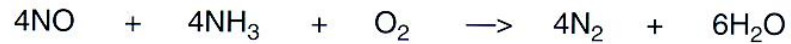


# NO<sub>x</sub> emissions model for Hemweg 8 plant

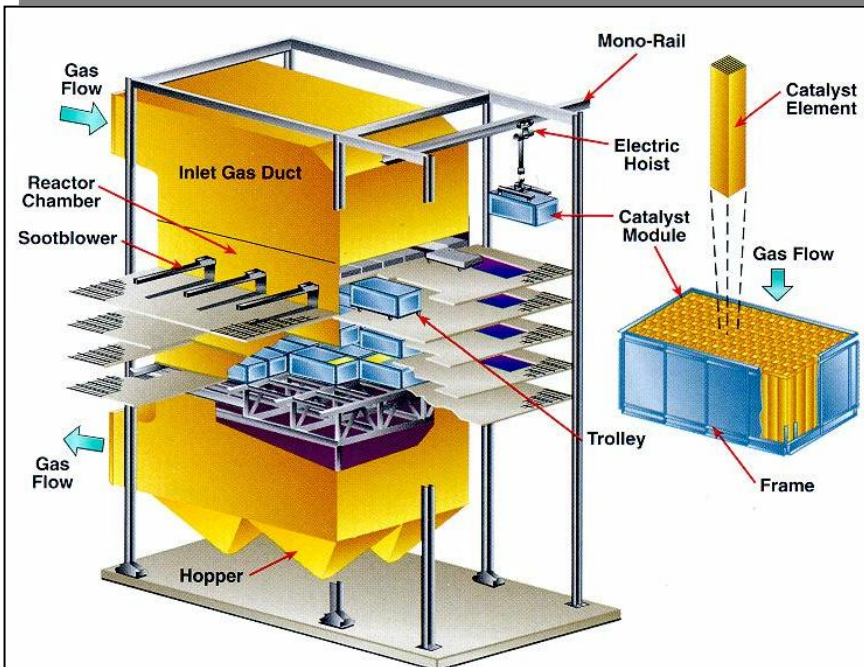
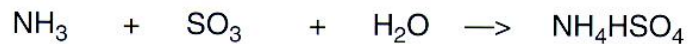
600 MWe, tangential, 1993, 535°C/568°/230 bar (between Amsterdam and Haarlem)



### Chemistry of the SCR Process



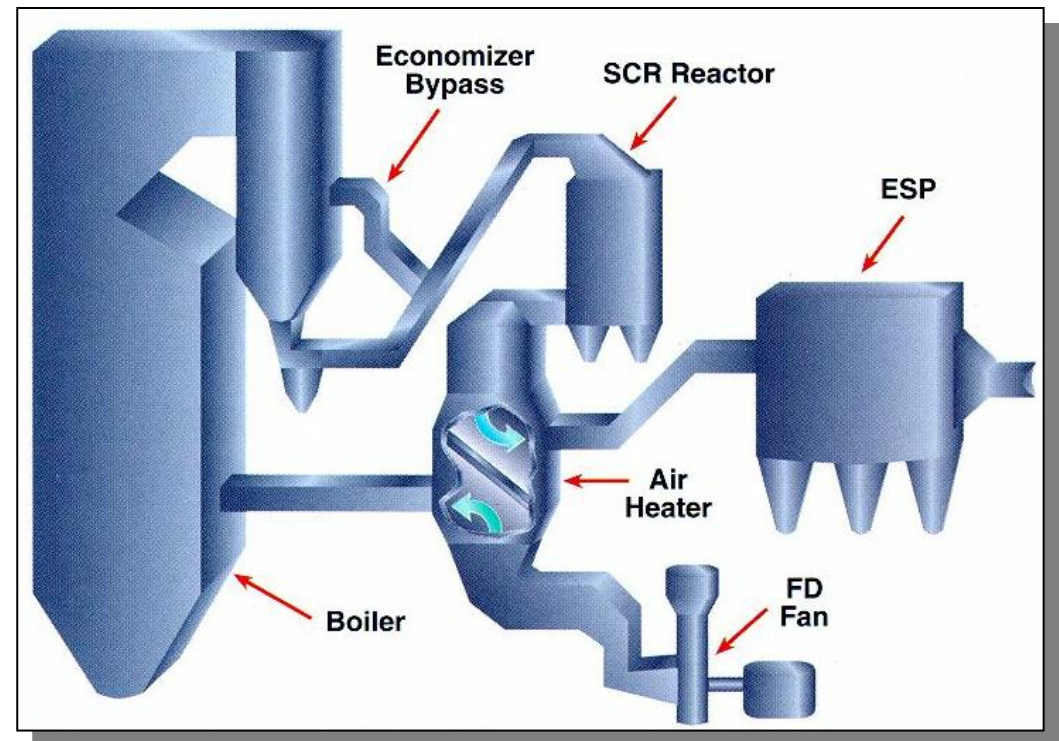
### Side Reactions



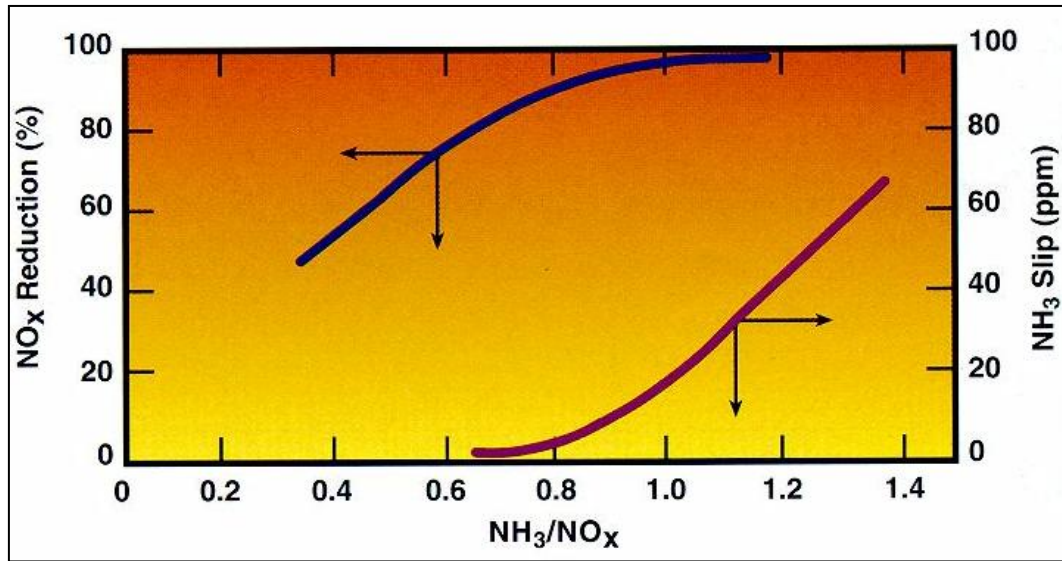
Vertical-flow fixed-bed type reactor chamber

## Selective catalytic reduction (SCR) of NO<sub>x</sub>

### /1

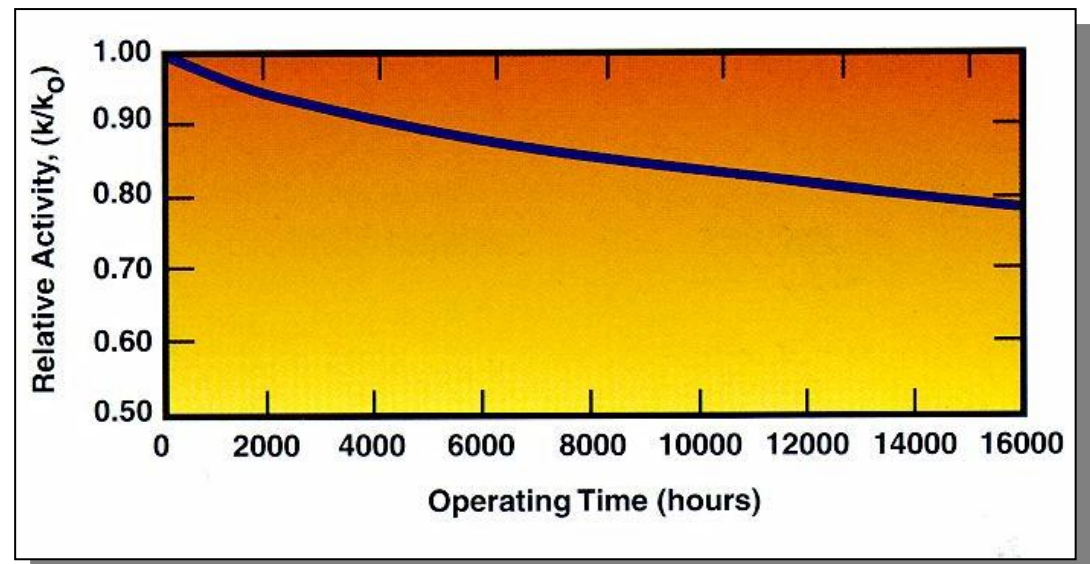






## Selective catalytic reduction (SCR) of $\text{NO}_x$ / 2

Efficiency and ammonia slip ( $\uparrow$ )  
and catalyst activity ( $\rightarrow$ )





## A damaged SCR unit: damaged catalyst



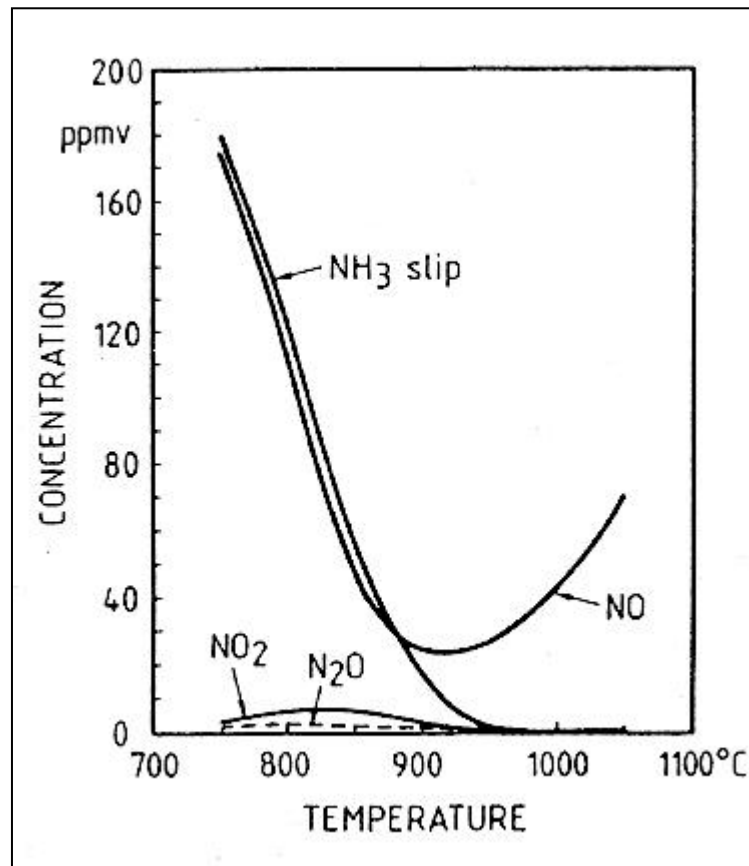
*Bild 2. Zerstrahlte Katalysatorsteine und leere Hülse.*



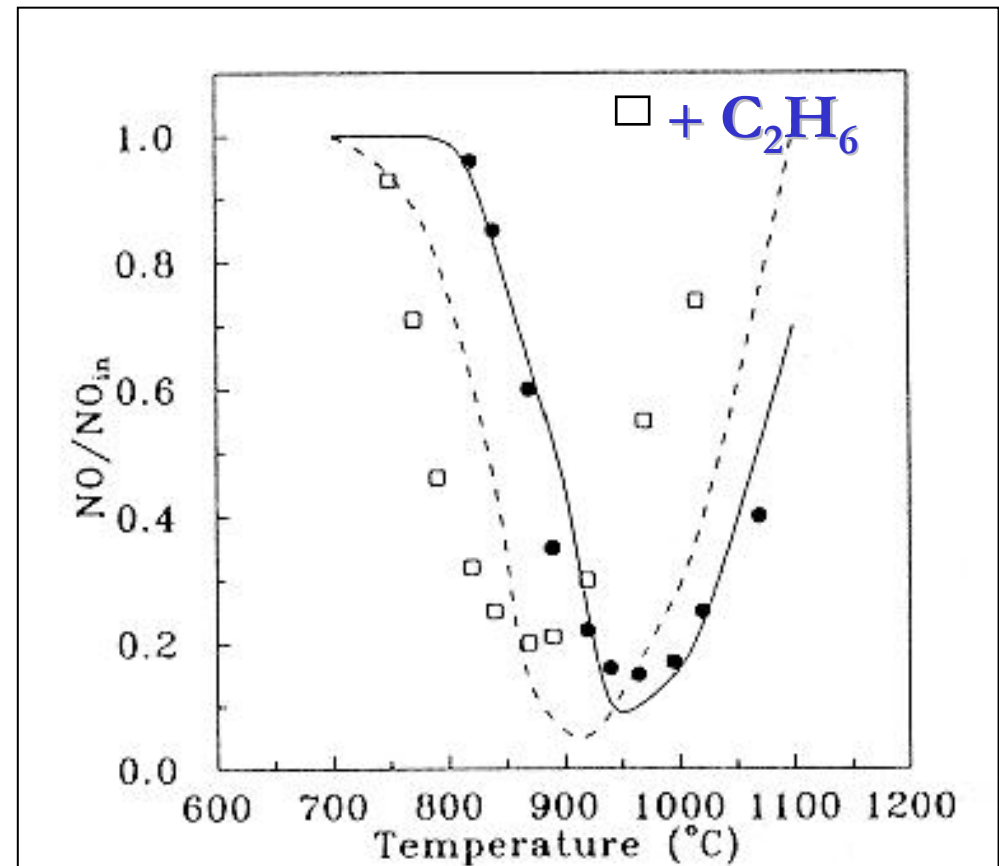
*Bild 3. Zerbrochener Katalysatorstein.*



# Selective Non-catalytic NO<sub>x</sub> reduction (SNCR)



Effect of temperature



Effect of C<sub>2</sub>H<sub>6</sub> addition





## NO<sub>x</sub> removal from flue gases : other methods

- Copper oxide process for simultaneous DeSO<sub>x</sub> / DeNO<sub>x</sub>
- dry absorption on activated carbon at ~220°C :



- Wet scrubbing with water after oxidation of NO



- Wet scrubbing with “chemical enhancement” (NaOH, KMnO<sub>4</sub>)
- Electron beam irradiation
- Phosphorous : catalyses oxidation of NO to NO<sub>2</sub>